ASX ANNOUNCEMENT 3 OCTOBER 2013

MAIDEN CAMELWOOD MINERAL RESOURCE

Rox Resources Limited

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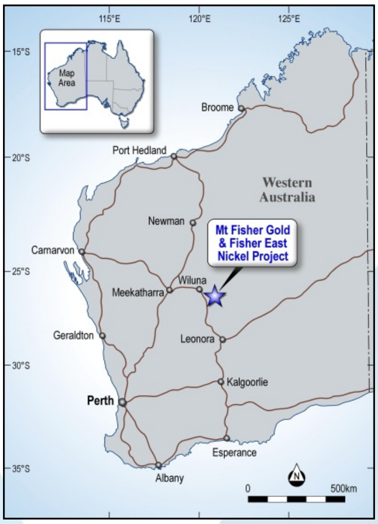
Projects:

Mt Fisher: nickel-gold (100%)

Reward: zinc-lead (49%)

Bonya: copper-silver (earning up to 70%)

Marqua: phosphate (100%)



- **Maiden Camelwood Mineral Resource of 1.6Mt @ 2.2% nickel**
- **Mineral Resource contains 34,600 tonnes of contained nickel**
- **40% of nickel metal content in higher confidence Indicated Mineral Resource category**
- **Higher grade core of 520,000 tonnes at 3.1% nickel**
- **Mineralisation open at depth and along strike**

Rox Resources Limited (**ASX: RXL**) ("**Rox**" or "**the Company**") is pleased to advise that it has completed the maiden September 2013 Mineral Resource estimate for the Camelwood nickel sulphide deposit.

The resource estimate comprises **1.6 million tonnes at 2.2% nickel** containing **34,600 tonnes of contained nickel.** Encouragingly 40% of the resource estimate sits in the higher confidence Indicated Mineral Resource category, using a 1.0% nickel lower cut-off (Table 1).

At the higher cut-off grade of 2.5% nickel the Mineral Resource contains **16,200 tonnes of nickel** with approximately 47.5% in the Indicated Mineral Resource category (Table 2). The resource at this higher cut-off grade is **520,000 tonnes at 3.1% nickel**.

Rox Managing Director, Mr Ian Mulholland commented "*We are highly encouraged by the maiden resource estimate at Camelwood which provides an excellent foundation on which the Company can build. It shows that there is a significant amount of nickel sulphide mineralisation at Camelwood, which remains open in all directions, and which should increase with further drilling*".

"Further drill testing of the Fisher East area is currently underway to explore for repeats of the Camelwood deposit. We remain confident that our exploration activities will unearth additional deposits across our extensive 655km^2 landholding at Mt Fisher. Deposits of the style of Camelwood do not typically occur in isolation. "

In further commentary Rox Chairman, Mr Jeff Gresham, stated *"to be able to complete an intensive drilling program and a resource estimate only nine months after its discovery is a significant achievement and a credit to the Rox team. Exploration and evaluation of the Mt Fisher nickel project is at a very early stage and I am confident that with further exploration and drilling the nickel resources will be significantly expanded."*

The Mineral Resource estimate has been completed in accordance with the guidelines of the JORC Code (2012 Edition). The tables to support the requirements of the JORC Code (2012 Edition) with regard to *Sampling Techniques and Data (Section 1), Reporting of Exploration Results (section 2),* and *Estimation and Reporting of Mineral Resources (Section 3)* are appended to this report.

Rox's database was audited by nickel sulphide specialist consultants Optiro Pty Ltd ("Optiro"), who also estimated the Mineral Resource in accordance with the JORC Code (2012 Edition) – see Appendix. A summary of the information used in the Mineral Resource Estimate follows.

The deposit is part of the Mt Fisher project and is located approximately 500 km north of Kalgoorlie in Western Australia. Camelwood is a nickel sulphide deposit hosted in an overturned sequence of felsic and ultramafic (plus mafic) units within a belt of arcuate greenstone units. Primary mineralisation consists of pyrrhotite + pentlandite (+ violarite) + pyrite sulphides in massive, semi-massive (net texture) or disseminated forms. The overall deposit style is similar to the Kambalda nickel sulphide deposits in Western Australia.

Discovered in December 2012, Camelwood has been sampled by reverse circulation (RC) and diamond drilling (DD) on an east-west grid pattern ranging from 50 m by 50 m to over 100 m by 100 m. A total of 28 RC holes (4,484 m) and 40 DD holes (14,401 m) were used to define the resource. Holes were generally angled towards the west at varying angles (between 60° and 90°) in order to optimally intersect the mineralisation. Currently mineralisation has been defined as relatively tabular zones, extending over a strike of 1,450 m and up to 500 m down-dip in the central part of the deposit. The thickness of the mineralisation is variable, ranging from 0.5 m to 15 m. The deposit is situated beneath a veneer (10-15m) of transported clays and deeply weathered gossan, while the sulphide mineralisation starts from about 90m below surface.

The main lithological units at Camelwood are a felsic hangingwall, ultramafic host and mafic footwall, all of which form an overturned package that strikes 345° and is moderately dipping (~60°-65°) to the east. The mineralisation is hosted within the ultramafic, immediately adjacent to the felsic (hangingwall) contact. Sulphide mineralisation has been modelled into disseminated, semi-massive (net) and massive sulphide domains, based on lithological logging. Two distinct lodes, the Main and North zones, have been defined, and have been domained using 0.5% Ni and 1.0% Ni cut-off grades. The grade cut-offs appear to correlate well with the disseminated and semi-massive/massive mineralisation boundaries. Three generations of cross-cutting felsic & mafic intrusives have been modelled, all of which transect the mineralisation. No major structural offsets are observed at Camelwood, although low angle/sub parallel shearing is evident in the drill core.

For the purpose of the estimation, all mineralised samples were composited to 1 m intervals, weighted by both length and density. Where density measurements were absent, a density regression calculation using nickel grade was applied.

Optiro generated a single block model with a parent cell size of 10 mE by 25 mN by 5 mRL, with sub-celling down to 0.5 mE by 1.25 mN by 0.25 mRL for adequate domain volume resolution. The estimate was completed in CAE Studio 3 (Datamine) using Ordinary Kriging. Five elements were estimated; Ni (%), As (ppm), S (%), Fe (%) and Mg (%), as well as specific gravity. All estimates were completed at the parent cell scale. Validation of the block model shows acceptable correlation of the input data to the estimated grades.

Grade continuity of the mineralisation at Camelwood is good, with a range of 270 m in the major direction in the nickel variogram. Due to the moderate-strong correlation of nickel with the other elements, the same search parameters were used for the estimation of each element. The search ranges were based on approximately half the range of the nickel variogram (150 m by 100 m by 8 m) in order to prevent over-smoothing of the local estimates. Three estimation search passes were used.

Hard estimation boundaries were applied between the Main and North domains, as well as between the 0.5% and 1.0 % Ni sub-domains. Between the oxidation interface one-way estimation boundaries were used, i.e. the estimation of the fresh material did not incorporate the oxidised or transitional composites but the oxide and transitional domains used all of the data. The premise for this is to acknowledge any secondary supergene enrichment of nickel within the oxide profile as it is not considered representative of the primary mineralisation. Violarite (a supergene nickel sulphide mineral) has been observed by the Rox geologists in drill spoils; however, this data was not captured in the logging and was therefore not incorporated into the interpretation of the oxide, transitional and fresh interfaces.

The Camelwood mineralisation has demonstrated sufficient continuity in both geological and grade areas to support the definition of Inferred and Indicated Mineral Resources in accordance with the *Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves* (the JORC Code, 2012 edition). Indicated Mineral Resources were classified using a nominal drilling density of less than 75 m by 75 m, well defined geological and grade continuity and a high level of confidence in the volume estimate of the mineralisation. In the case of Inferred Mineral Resources, the criteria include a nominal drilling density of greater than 75 m by 75 m and a lower confidence in the geological continuity and volume definition (Figure 1). Approximately 12 % of the total resource has been extrapolated (i.e. the nickel has been estimated in search pass three or assigned), with minimal extrapolation distances beyond drillholes.

Optiro carried out a site visit to the Camelwood deposit on 22-23 July 2013. Mark Drabble (Principal Consultant), who is acting as Competent Person, inspected the deposit area, the core logging and sampling facilities.

Ian Mulholland

IAN MULHOLLAND
Managing Director

Table 1: Camelwood Mineral Resource reported at a 1.0% nickel cut-off

	Camelwood Mineral Resource - September 2013		
	Tonnes (Mt)	Grade	Contained Metal
		Ni %	Nickel (kt)
Indicated Mineral Resource			
Oxide	-	-	-
Transitional	-	-	-
Fresh	0.6	2.4	13.8
Total Indicated	**0.6**	**2.4**	**13.8**
Inferred Mineral Resource			
Oxide	0.03	1.7	0.5
Transitional	0.02	1.7	0.7
Fresh	0.9	2.1	19.6
Total Inferred	**1.0**	**2.1**	**20.8**
Total	**1.6**	**2.2**	**34.6**

Table 2: Camelwood Mineral Resource reported at a 2.5% nickel cut-off

	Camelwood Mineral Resource - September 2013		
	Tonnes (Mt)	Grade	Contained Metal
		Ni %	Nickel (kt)
Indicated Mineral Resource			
Oxide	-	-	-
Transitional	-	-	-
Fresh	0.2	3.2	7.7
Total Indicated	**0.2**	**3.2**	**7.7**
Inferred Mineral Resource			
Oxide	-	-	-
Transitional	-	-	-
Fresh	0.3	3.0	8.4
Total Inferred	**0.3**	**3.0**	**8.4**
Total	**0.5**	**3.1**	**16.2**

Figure 1: Camelwood Prospect Drill Long Section showing Resource Categories (Orange = Indicated, Green = Inferred)

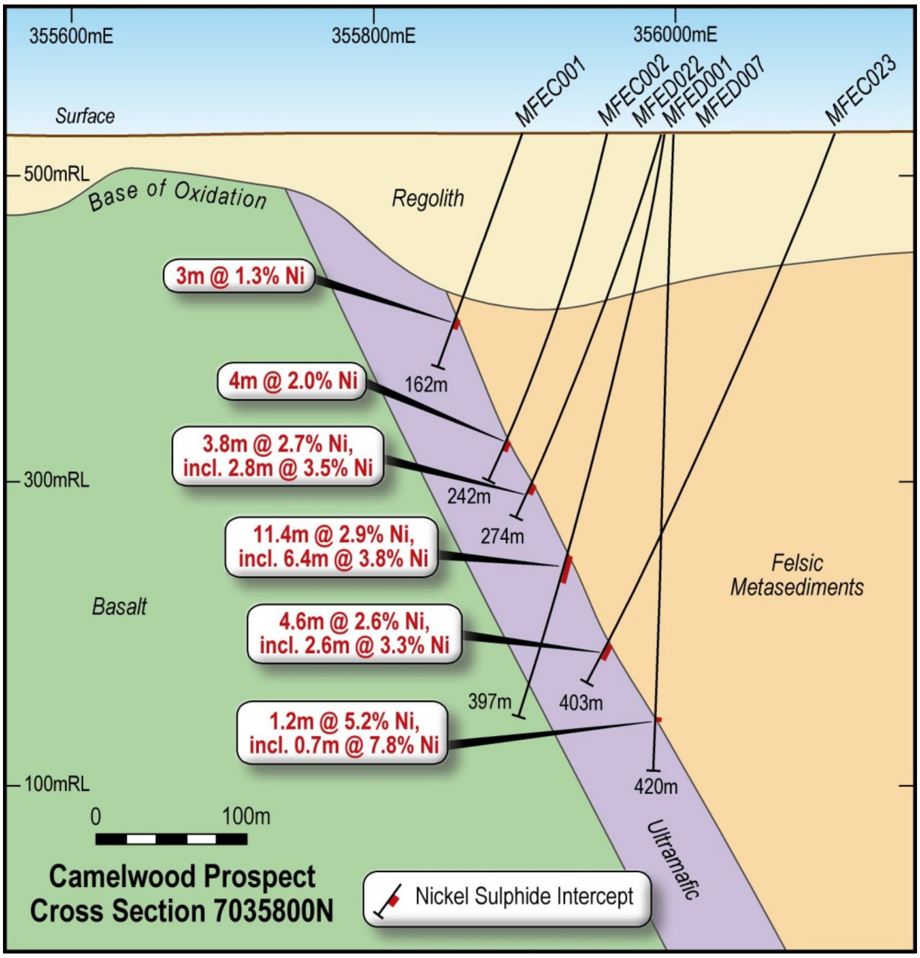


Figure 2: Cross Section 7035800N through the Camelwood deposit

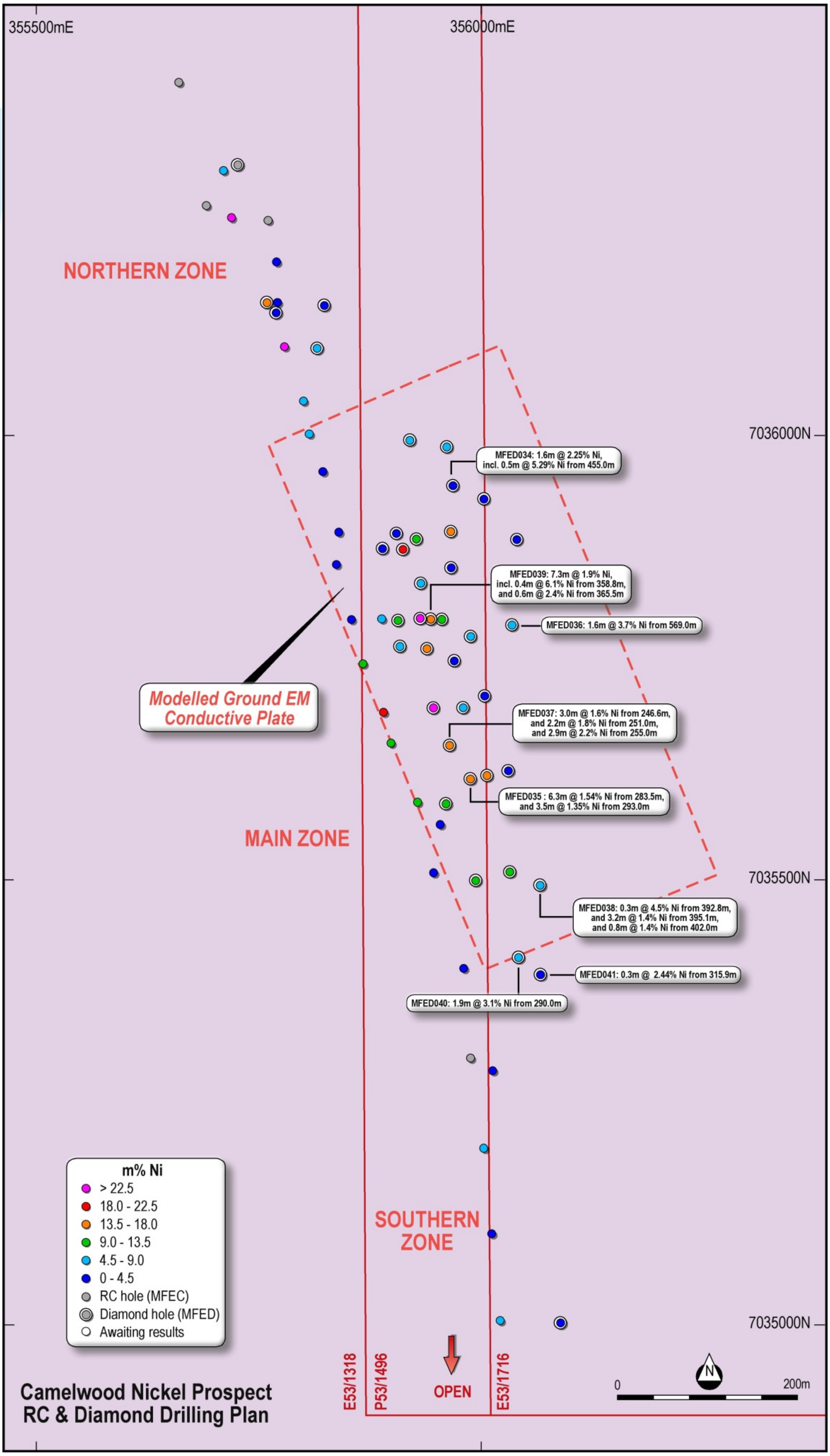


Figure 3: Camelwood Deposit Drill Plan

Table 3: Camelwood Mineral Resource Estimate at Various Cut-Off Grades

Ni% cut-off	Category	Tonnes (Mt)	Grade		Contained Metal
			Ni%	S%	Nickel (kt)
0.5	Indicated	0.68	2.2	9.8	14.7
	Inferred	1.89	1.4	6.1	27.3
	Total	**2.56**	**1.6**	**7.1**	**42.0**
1.0	Indicated	0.57	2.4	11.0	13.8
	Inferred	1.00	2.1	9.4	20.8
	Total	**1.57**	**2.2**	**10.0**	**34.6**
1.5	Indicated	0.51	2.6	12.0	13.1
	Inferred	0.79	2.3	10.4	18.0
	Total	**1.29**	**2.4**	**11.0**	**31.0**
2.0	Indicated	0.38	2.8	14.1	10.8
	Inferred	0.42	2.8	12.6	11.6
	Total	**0.80**	**2.8**	**13.3**	**22.4**
2.5	Indicated	0.24	3.2	16.8	7.7
	Inferred	0.28	3.0	14.2	8.5
	Total	**0.52**	**3.1**	**15.4**	**16.2**
3.0	Indicated	0.13	3.6	19.7	4.6
	Inferred	0.15	3.3	16.0	4.8
	Total	**0.27**	**3.4**	**17.7**	**9.4**
3.5	Indicated	0.05	4.1	23.0	2.2
	Inferred	0.02	4.0	20.9	1.0
	Total	**0.08**	**4.1**	**22.3**	**3.2**

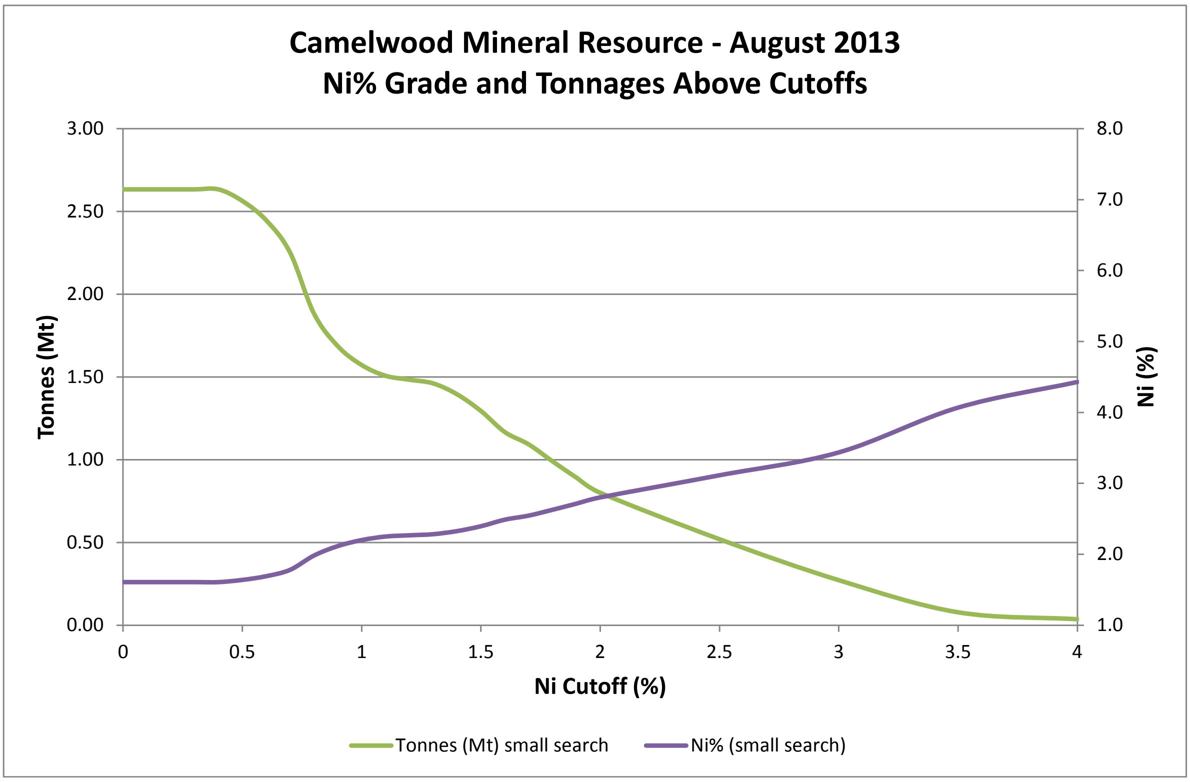


Figure 4: Grade Tonnage Curve Based on Data listed in Table 3

Table 4: Camelwood Diamond Drilling Results

Hole	East	North	Depth (m)	Dip	Azimuth	From (m)	To (m)	Interval	Ni%	m%
MFED001	355997	7035799	397.3	-75	270	282.6	294.0	11.4	2.93	33.4
		Including				282.6	289.0	6.4	3.80	
		Including				282.6	285.5	2.9	4.66	
MFEC002	355996	7035702	261.5	-75	270	211.7	228	16.3	1.79	29.2
		Including				211.7	218	6.3	2.53	
		Including				212.0	212.47	0.47	5.42	
MFED003	355991	7035593	210.9	-80	270	178.3	185.8	7.5	1.22	9.2
		Including				178.3	178.7	0.4	3.76	
MFED004	355900	7036097	216.1	-60	270	197.3	214.4	17.1	0.47	8.0
MFED005	355995	7035900	421.3	-78	270	382.0	387.7	5.7	2.25	12.8
		Including				*382.0*	*382.4*	*0.4*	*5.38*	
		And				*384.6*	*387.7*	*3.1*	*3.37*	
		Including				*384.6*	*386.3*	*1.7*	*4.64*	
MFED006	355995	7035900	346.2	-70	270	317.7	319.0	1.3	2.55	3.3
		Including				317.7	318.3	0.6	3.76	
MFED007	356000	7035795	421.1	-85	270	388.7	389.9	1.2	5.20	6.2
		Including				388.7	389.4	0.7	7.79	
MFED008	355999	7035850	376.3	-80	270	350.5	352.3	1.8	2.81	5.1
		Including				350.5	350.8	0.30	4.03	
MFED009	355999	7035850	426.9	-85	270	401.66	403.70	2.04	1.61	3.3
		Including				*401.66*	*401.88*	*0.22*	*3.49*	
		And				*402.75*	*403.70*	*0.95*	*2.60*	
MFED010	355999	7035850	367.2	-72	270	341.11	347.26	6.15	3.30	20.3
		Including				*341.11*	*341.38*	*0.27*	*3.43*	
		And				*341.66*	*341.85*	*0.19*	*10.97*	
		And				*342.25*	*347.26*	*5.01*	*3.43*	
		Including				*342.25*	*343.89*	*1.64*	*5.81*	
MFED011	355999	7035850	316	-62	270	293.71	293.98	0.27	1.88	0.5
MFED012	355996	7035702	427.1	-90	270	375.68	376.42	0.74	3.84	2.8
MFED013	355823	7036149	171.45	-65	270	140.87	141.55	0.68	5.88	4.0
MFED014	355823	7036149	162.3	-55	270	130.60	138.00	7.40	1.89	14.0
		Including				*130.60*	*132.05*	*1.45*	*3.60*	
MFED015	355859	7036150	240.85	-78	270	202.45	202.91	0.46	1.47	0.9
		And				217.32	217.52	0.20	1.04	
MFED016	355816	7036302	297.95	-60	270	NSR				
MFED017	355900	7036698	751.05	-60	270	NSR				
MFED018	355995	7036000	450.4	-85	270	414.98	416.63	1.65	3.19	5.6
		And				417.63	417.83	0.20	1.55	
MFED019	355999	7036000	369.5	-74	270	340.69	344.00	3.31	1.88	6.2
		Including				*340.69*	*341.54*	*0.85*	*5.01*	
MFED020	356000	7035749	309.3	-75	270	269.7	277.0	7.3	1.94	14.2
		Including				*269.7*	*275.0*	*5.3*	*2.40*	

		Including				*269.7*	*270.2*	*0.5*	*6.67*	
MFED021	355999	7035749	249.9	-62	270	226.0	229.0	3.0	1.94	5.7
		Including				*226.0*	*227.0*	*1.0*	*3.36*	
MFED022	356109	7035796	274	-70	270	246.2	250.0	3.8	2.73	10.3
		Including				*246.2*	*249.0*	*2.8*	*3.49*	
MFED023	356106	7035799	403	-65	270	377.4	382.0	4.6	2.58	12.0
		Including				377.4	380.0	2.6	3.28	
		Including				377.4	377.9	0.5	4.98	
		And				379.0	380.0	1.0	4.26	
MFED024	356241	7035612	435.3	-60	270	409.8	410.3	0.5	6.44	3.2
MFED025	356241	7035612	401.4	-50	270	373.8	380.8	7.0	2.40	16.8
		Including				*373.8*	*378.0*	*4.2*	*3.17*	
MFED026	356195	7035903	504.5	-65	270	483.0	485.7	2.7	5.20	14.0
		Including				*483.9*	*485.7*	*1.8*	*6.30*	
MFED027	356110	7035698	346.0	-65	270	317.3	320.4	3.1	2.11	6.5
		Including				*317.3*	*317.8*	*0.5*	*4.27*	
MFED028	356197	7035899	550.0	-73	270	522.8	523.0	0.2	5.29	1.3
MFED029	356184	7035754	448.0	-57	270	406.4	407.2	0.8	3.40	2.7
MFED030	356135	7035002	250.0	-75	270	233.95	235	1.05	0.48	0.5
MFED031	356153	7035951	535.9	-72	270	496.85	497.1	0.25	9.01	2.2
MFED032	356151	7035503	373.2	-65	270	312.7	316.1	3.4	2.74	9.3
		Including				*314.6*	*316.1*	*1.5*	*4.11*	
MFED033	356151	7035503	284.9	-51	270	265.2	268.4	3.2	3.39	10.9
		Including				*265.6*	*268.4*	*2.8*	*3.72*	
MFED034	356153	7035951	484.0	-65	270	455.0	456.6	1.6	2.25	3.6
		Including				*455.0*	*455.5*	*0.5*	*5.29*	
MFED035	356132	7035600	306.5	-58	270	283.5	289.8	6.3	1.54	14.3
		And				293.0	296.5	3.5	1.35	
MFED036	356363	7035800	604.5	-58	270	569.0	570.6	1.6	3.69	6.1
MFED037	356065	7035650	276.3	-65	270	246.6	249.6	3.0	1.58	15.1
		Including				*246.6*	*247.7*	*1.1*	*3.21*	
		And				251.0	253.2	2.2	1.79	
		And				255.0	257.9	2.9	2.21	
MFED038	356270	7035500	433.0	-64	270	392.8	393.1	0.3	4.52	7.0
		And				395.1	398.3	3.2	1.43	
		Including				*395.1*	*395.5*	*0.4*	*3.76*	
		And				402.0	402.8	0.8	1.38	
MFED039	356094	7035790	381.8	-60	270	358.8	366.1	7.3	1.88	13.6
		Including				*358.8*	*364.4*	*5.6*	*2.13*	
		Including				*358.8*	*359.2*	*0.4*	*6.05*	
		And				365.5	366.1	0.6	2.43	
MFED040	356180	7035398	322.0	-60	270	290.0	291.9	1.9	3.11	5.8
MFED041	356181	7035398	346.8	-72	270	315.9	316.2	0.3	2.44	0.7

Table 5: Camelwood RC Drilling Results

Hole	East	North	Depth (m)	Dip	Azimuth	From (m)	To (m)	Interval	Ni%	m%
MFEC001	355899	7035798	162	-70	270	130	133	3	1.27	3.8
		Including				*130*	*132*	*2*	*1.58*	
MFEC002	355956	7035802	242	-75	270	212	216	4	1.99	8.0
MFEC003	355986	7035594	172	-65	270	141	146	5	1.45	12.4
		And				152	155	3	1.72	
		Including				*152*	*154*	*2*	*2.22*	
MFEC004	355974	7035692	182	-60	270	159	179	20	1.06	21.2
		Including				*159*	*165*	*6*	*1.36*	
		Including				*169*	*174*	*5*	*1.49*	
MFEC005	355903	7035893	187	-60	270	147	148	1	2.99	3.0
MFEC006	355994	7035506	150	-65	270	126	126	1	2.48	2.5
MFEC007	355854	7035998	150	-60	270	118	121	3	1.82	5.5
MFEC010	355829	7036103	150	-60	270	118	136	18	1.53	27.5
		Including				*119*	*128*	*9*	*2.04*	
MFEC012	355832	7036200	168	-70	270	153	154	1	1.10	1.1
MFEC013	355818	7036247	162	-60	270	Terminated short of target				
MFEC015	355845	7036059	162	-60	270	125	130	5	1.33	6.7
MFEC016	355881	7035958	156	-60	270	129	133	4	1.11	4.4
MFEC017	355720	7036259	86	-60	270	NSR (gossanous 56-65m)				
MFEC020	355928	7035750	174	-60	270	141	146	5	1.80	12.0
		Including				*141*	*143*	*2*	*2.49*	
		And				157	159	2	1.49	
MFEC021	355769	7036249	150	-60	270	105	124	19	1.32	25.1
MFEC022	355933	7035854	216	-60	270	186	187	1	2.55	2.6
MFEC023	355750	7036300	141	-60	270	101	120	19	0.44	8.4
MFEC024	355970	7035650	186	-60	270	144	148	4	1.27	9.2
		And				155	159	4	1.04	
MFEC025	355697	7036402	130	-60	270	NSR				
MFEC026	356000	7035397	138	-75	270	111	112	1	1.13	1.1
MFEC027	356003	7035300	102	-75	270	NSR (gossanous 78-79m)				
MFEC028	355993	7035558	156	-70	270	146	148	2	1.36	2.7
MFEC029	356054	7035294	150	-65	270	134	135	1	1.22	1.2
MFEC030	356058	7035199	156	-60	270	140	144	4	1.90	7.6
		Including				*140*	*141*	*1*	*2.84*	
MFEC031	356059	7035096	140	-60	270	124	126	2	1.12	2.2
MFEC032	355826	7036155	174	-60	270	144	146	2	2.02	4.0
MFEC033	356070	7035001	138	-60	270	119	121	2	3.50	7.0
		Including				*119*	*120*	*1*	*5.71*	

Notes:

- Grid coordinates GDA94: Zone 51, Collar positions determined by hand held GPS and confirmed by DGPS.
- All holes RL 537 AHD confirmed by DGPS.
- Hole azimuths planned to be 270 degrees, but hole deviations may result in hole paths different to those intended. Correct lateral positions of down hole intercepts are shown on the Figures.
- RC drilling (hole prefix MFEC) by reverse circulation face sampling hammer, then 1 metre samples split and bagged.
- Diamond drilling (hole prefix MFED) by HQ/NQ diamond core, with core cut in half and sampled to either significant geological boundaries or even metre intervals.
- Diamond drill samples weighed in water and air to determine bulk density, and then crushed to 6.5mm
- 3-5kg sample preparation by pulp mill to nominal P80/75um.
- Ni assays by ICP-OES following a 4 acid digest (Intertek analysis code 4A/OE).
- Certified Reference Standards and field duplicate samples were inserted at regular intervals to provide assay quality checks. Review of the standards and duplicates are within acceptable limits.
- Cut-off grade 1% Ni with up to 2m of internal dilution allowed (with the exception of holes MFED004 & MFEC023).
- Given the angle of the drill holes and the interpreted 60 degree dip of the host rocks, reported intercepts will be more than true width.

Appendix

The following information is provided to comply with the JORC (2012) requirements for the reporting of the Camelwood Mineral Resource estimate on tenements E53/1318, E53/1716 and P53/1496.

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	*Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*	The Camelwood deposit has been sampled in a nominal 50 m by 50 m to 100 m by 100 m spacing using a combination of 5.5" (140 mm) reverse circulation percussion (RC) and diamond (DD) drillholes. The core size is dominantly NQ2 size diameter, and two HQ size holes were drilled (including 1 metallurgical). The summary of drilling used in the Mineral Resource is 30 RC holes for 4,688 m, and 41 DD holes for 15,152.2 m. Holes were angled towards grid west at varying angles to intersect the mineralised zones at close to perpendicular.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used	Drillhole locations were picked up by a licenced surveyor for holes MFED001 to MFED017 and RC holes MFEC001 to MFEC024. The remaining holes have been picked up by Rox using a Differential GPS unit with an accuracy of <0.3m. RC samples were collected by riffle or cone splitters. The majority of the Camelwood Mineral Resource is defined by diamond core drilling, which was logged for lithology, structure, alteration, geotechnical and other attributes. The Rox sampling protocols and QAQC have been reviewed by Optiro and are as per industry best practice procedures.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information	Diamond core is dominantly NQ2 size, sampled on geological intervals, with a minimum of 0.1 m up to a maximum of 1.5 m. NQ2 core is cut into half, or quarter for HQ holes. RC drillholes were sampled on 1m intervals using riffle or cone splitter units. Samples were sent to Intertek Genalysis in Kalgoorlie, crushed to 10mm, dried and pulverised (total prep) in LM5 units (Some samples > 3kg were split) to produce a sub-sample. The pulps were then sent to Perth for analysis by four acid digest with a multi-element ICP-OES finish (code: 4A/OE-multi element). Au, Pt and Pd were analysed by 50 gram fire assay with a mass spectrometer finish. Internal laboratory QA uses CRM's, blanks, splits and replicates, along with 10% repeats.
Drilling techniques	*Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	Drilling techniques were Reverse Circulation (RC) and diamond core (DD). The RC hole diameter was 140mm face sampling hammer. Hole depths range from 100m to 220m. DD hole diameter was mostly NQ2 with HQ pre-collar and upper hole portions. Two full holes were drilled HQ. Hole depths range from 140m to 640m. The core was orientated using a Camtech orientation tool. Pre-collars for diamond holes were drilled using a roller bit and reamed to HW casing size.
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed*	Diamond drill core recoveries were logged and recorded in the database. Overall recoveries were >95%, and there were no significant core loss or recovery problems. RC drill recoveries varied, with wet samples (generally below 150m depth) presenting lower sample recoveries.
	Measures taken to maximise sample recovery and ensure representative nature of the samples	Diamond core was reconstructed into continuous sample runs on an angle iron used for orientation marking. Depths are measured and checked against marked depths on the core blocks. RC samples were visually checked for recovery, moisture and contamination and notes made in the logs.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Most of the samples used in the Mineral Resource estimate come from diamond core drilling which had high recoveries. There is no observable relationship between recovery and grade, and therefore no sample bias.

Criteria	JORC Code explanation	Commentary
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	Detailed geological and geotechnical logs were carried out on all diamond drill holes for recovery, RQD, structures etc. which included structure type, dip, dip direction, alpha angle, beta angle, texture, shape, roughness, fill material, and this data is stored in the database.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.	Logging of diamond core and RC chips recorded lithology, mineralogy, mineralisation, structure (DD only), weathering, colour, and other sample features. Core was photographed both wet and dry and is stored in plastic core trays. RC chips are stored in plastic RC chip trays.
	The total length and percentage of the relevant intersections logged	All holes were logged in full except for the rock roller bit diamond hole pre-collars (0-120m in most cases).
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.*	Drill core was cut in half on site using a core saw. All samples were collected from the same side of the core, preserving the orientation mark in the kept core half.
	If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.	RC samples were collected on the drill rig using a cone splitter. Some of the mineralised samples were collected wet, and these were noted in the drill logs and database.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	The sample preparation followed industry best practice. This involved oven drying, coarse crushing of diamond core to ~10mm, followed by pulverisation of the entire sample in an LM5 or equivalent pulverising mill to a grind size of 85% passing 75 micron.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Field QC procedures involve the use of Certified Reference Materials (CRM's) as assay standards, along with blanks, duplicates and barren waste samples. The insertion rate of these was approximately 1:50.
	Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.	No diamond core field duplicates were taken. For RC drilling field duplicates were only taken on a routine basis at an approximate 1:20 ratio using the same sampling techniques (i.e. cone splitter) and inserted into the sample run for the first 5 holes. After that no field duplicates were taken.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	The sample sizes are considered more than adequate to ensure that there are no particle size effects relating to the grain size of the mineralisation which lies in the percentage range.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	The analytical technique involved a four acid digest followed by multi-element ICP/OES analysis (Intertek analysis code 4A/OE). The four acid digest involves hydrofluoric, nitric, perchloric and hydrochloric acids and is considered a "complete" digest for most material types, except certain chromite minerals.
	For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	No geophysical or portable analysis tools were used to determine assay values stored in the database.
	Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	Internal laboratory control procedures involve duplicate assaying of randomly selected assay pulps as well as internal laboratory standards. All of these data are reported to the Company and analysed for consistency and any discrepancies. Check assays were undertaken at an independent third party assay laboratory and correlated extremely well.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.*	Both senior technical personnel from the Company (Managing Director, Chairman and Exploration Manager) and the Principal Consultant Geologist from Optiro have visually inspected and verified the significant drill core intersections.
	The use of twinned holes.	One RC hole was twinned when it was suspected that downhole contamination had occurred. The contamination was confirmed with a twin RC hole as well, and the original RC hole and all associated results were deleted from the database.

Criteria	JORC Code explanation	Commentary
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Primary data was collected using a standard set of Excel templates on Toughbook laptop computers in the field. These data are transferred to Geobase Pty Ltd for data verification and loading into the database.
	Discuss any adjustment to assay data.	No adjustments or calibrations have been made to any assay data.
Location of data points	*Accuracy and quality of surveys used to locate drillholes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	Initial drill hole surveying was carried out by Phil Richards, licensed surveyor for holes MFED001-017 and MFEC001-024. Subsequent surveying was undertaken by the Company using a Digital GPS unit check surveys made of the base station and previously surveyed drill hole locations.
	Specification of the grid system used.	The grid system is MGA_GDA94, zone 51 for easting, northing and RL.
	Quality and adequacy of topographic control.	The topographic surface was generated from drill collar surveys and also digital terrain models generated from low level airborne geophysical surveys.
Data spacing and distribution	*Data spacing for reporting of Exploration Results.*	The nominal drill hole spacing is 100 x 100 metres, with some areas closed into 50 x 50 metre spacing.
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	The mineralisation and geology showed very good continuity from hole to hole and is sufficient to support the definition of a Mineral Resource or Ore Reserve and the classifications contained in the JORC Code (2012 Edition).
	Whether sample compositing has been applied.	No sample compositing has occurred for diamond core drilling. Sample intervals are based on geological boundaries with even one metre samples between. For RC samples, sample compositing occurred over 4 metre intervals for non-mineralised material, but all mineralised intervals were sampled at a one metre interval.
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	The deposit strikes at about 345 degrees and dips to the east at between -60 to -65 degrees. The drill orientation was planned to be 270 degrees, so slightly oblique to the perpendicular direction, however, many drill holes swung slightly south (to about 255 degrees) so were drilling essentially perpendicular to strike. This is confirmed in structural logging of mineralised zones.
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	No sampling bias is believed to have been introduced.
Sample security	*The measures taken to ensure sample security.*	Sample security is managed by the Company. After preparation in the field samples are packed into polyweave bags and despatched to the laboratory. For a large number of samples these bags were transported by the Company directly to the assay laboratory. In some cases the sample were delivered to a transport contractor who then delivered the samples to the assay laboratory. The assay laboratory audits the samples on arrival and reports any discrepancies back to the Company. No such discrepancies occurred.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	A review of the sampling techniques and data was carried out by Optiro as part of the Mineral Resource estimate. The database is considered by Optiro to be of sufficient quality to support the Mineral Resource estimate. In addition, from time to time, the Company carries out its own internal data audits.

Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.	Camelwood is located within Exploration License E53/1318, E53/1716 and Prospecting License P53/1496. Rox Resources holds an option to purchase P53/1496 and E53/1318 which are held by Gerard Victor Brewer. E53/1716 is 100% owned by Rox Resources Limited.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	The tenements are all in good standing and no known impediments exist.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	No previous exploration has been done at the Camelwood prospect.
Geology	Deposit type, geological setting and style of mineralisation.	The geological setting is of Archaean aged komatiite system, bounded by hangingwall basaltic rocks and footwall felsic metasediments. Mineralisation is mostly situated at the (eastern) basal ultramafic - felsic contact. The rocks are strongly talc-carbonate altered. Metamorphism is mid-upper Greenschist. The deposit is analogous to Kambalda style nickel sulphide deposits.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: • easting and northing of the drill hole collar • elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar • dip and azimuth of the hole • down hole length and interception depth • hole length.	Refer to drill results tables 4 & 5 and the Notes attached thereto.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.	All reported assay intervals have been length weighted. No top cuts have been applied. A lower cutoff of 1% is applied with up to 2m of internal dilution allowed. See Notes to Tables 4 & 5.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	High grade massive sulphide intervals internal to broader zones of mineralisation are reported as included intervals. See Tables 4 & 5.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalent values have been used or reported.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').	The mineralisation at Camelwood is moderately east dipping throughout the deposit. Drillhole azimuths are planned at 270^0 and are inclined between -50^0 and -90^0 degrees. Given the angle of the drill holes and the interpreted -60^0 dip of the host rocks and mineralisation, reported intercepts will be more than true width.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Refer to Figures 1-3 in the text.

Criteria	JORC Code explanation	Commentary
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	All results are reported
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	All core samples are measured for bulk density by the laboratory using the water displacement method. Multi element assaying on all samples was carried out for a suite of potentially deleterious elements such as Arsenic and Magnesium. Geotechnical data was collected from all diamond drillholes including recovery and RQD. Structural information was recorded; structure type, thickness, lithology, and alpha/beta angles (dip and dip direction).
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive	Further work is being planned for extensional diamond drilling at Camelwood. Metallurgical sighter testwork is currently being carried out on both massive and disseminated ore types by METs Pty Ltd.

Section 3 Estimation and Reporting of Mineral Resources

Criteria	JORC Code explanation	Commentary
Database integrity	Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.	Data templates with lookup tables and fixed formatting are used for logging and sampling data recording. Data transfer is via email with a copy sent to both the Company and the external database consultant. Sample numbers are unique and pre-numbered bags are used. These procedures minimise any potential errors.
	Data validation procedures used.	Data validation checks are run by Geobase, and they maintain a “master copy” of the database. The Company uses working copies which are provided by Geobase on a regular basis.
Site visits	Comment on any site visits undertaken by the Competent Person and the outcome of those visits.	Mark Drabble, who is acting as Competent Person for the Mineral Resource estimate visited the Camelwood site on 22-23 July 2013 and inspected the core logging and sample preparation facilities. A number of minor recommendations were made to improve procedures, but no major issues were encountered.
	If no site visits have been undertaken indicate why this is the case.	Not applicable.
Geological interpretation	Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.	There is a high degree of confidence in the geological model of the Camelwood deposit, based on consistent stratigraphy in drill holes and highly correlatable rock units and mineralisation. The nickel sulphide mineralisation consistently occurs at the basal contact of an ultramafic flow with the footwall felsic sediment.
	Nature of the data used and of any assumptions made.	Petrography and lithogeochemistry have been used to assist in the identification and characterisation of the rock units.
	The effect, if any, of alternative interpretations on Mineral Resource estimation.	The geological model is simple and no alternative interpretations of geology exist. Infill drilling has supported the continuity of the geological model.
	The use of geology in guiding and controlling Mineral Resource estimation.	The key geological control on the Mineral Resource estimate is the logging of massive versus disseminated sulphide zones. This was a critical factor in domaining the mineralisation so that assay smoothing across this resource “hard boundary” did not occur.

Criteria	JORC Code explanation	Commentary
	The factors affecting continuity both of grade and geology.	There was good continuity of grade domains (indicated by the nickel variogram Major direction range of 270 metres) and geological domains. However, great care was taken to properly domain the sulphide mineralisation types (massive vs. disseminated) as described above.
Dimensions	The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource	The mineralisation at Camelwood extends over a 1,400 metre strike length, starting at about 90-100 metres below ground surface (below the completely oxidised zone) and has been drilled to over 500 metres depth. The deposit is still open along strike and at depth. Drilling has penetrated adequately on both sides of the mineralised zone to define it well.
Estimation and modelling techniques	The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.	Nickel mineralisation at Camelwood was modelled as four domains using nickel grade cut-offs and geology. They included; Main 0.5%, Main 1.0%, North 0.5% and North 1.0%. Grade estimation was completed using Ordinary Kriging (OK). CAE Studio 3 software was used to estimate five elements; Ni%, S%, Fe%, Mg% and As (ppm), as well as specific gravity. Drillhole sample data was flagged using domain codes generated from three dimensional mineralisation domains and oxidation surfaces. Sample data was composited downhole to 1 m intervals using a best fit method, and was weighted by length and density. A regression technique was used to assign density values where measurements were unavailable for compositing. Intervals with no assays were excluded from the compositing routine, and intervals with below detection results were reset to half detection values. The influence of extreme sample distribution outliers were reduced by top-cutting, where required. The top-cut values were determined using a combination of top-cut analysis tools, including grade histograms, log probability plots and population statistics. Top cuts were reviewed and applied on a domain basis. Variography was completed in 3D space using the fresh composites within the Main domains only due to the small number of samples. Directional variograms were modelled using normal scores transformations. Nugget values ranged from 0.04 for Mg to 0.35 for Ni . Grade continuity was variable depending on the element and ranged from 125 m to 280 m in the major direction.
	The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.	This is the maiden Mineral Resource for the Camelwood deposit. No previous mining activity has taken place.
	The assumptions made regarding recovery of by-products.	No recovery assumptions have been built into the model.
	Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).	The non-grade elements estimated are As (ppm), Fe%, Mg% and S%.

Criteria	JORC Code explanation	Commentary
	In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.	A single block model for Camelwood was constructed using an 10 mE by 25 mN by 5 mRL parent block size with subcelling to 0.5 mE by 1.25 mN by 0.25 mRL for domain volume resolution. Estimation was completed at the parent cell scale. Kriging neighbourhood analysis was carried out in order to optimise the block size, search distances and sample numbers used. Discretisation was set to 4 by 10 by 2 for all domains. The size of the search ellipse per domain was set to approximately half the ranges of the nickel variography to minimise the extrapolation of lower grade intervals and therefore improve the local estimate. The search ellipse was set to 150 m in the major direction by 100 m in the semi-major direction by 8 m in the minor direction and was kept constant for all elements due to the moderate to strong correlation between elements. Three search passes were used for each domain. In general, the first pass was set at 150 m by 100 m by 8 m with a minimum of 8 samples in the Main and 6 samples in the North domains, using an overall maximum of 32 samples. In the second pass the search ranges were unchanged, but the minimum number of samples was reduced to 4 samples for all domains. The third pass ellipse was extended to 10 times the initial search ellipse and a minimum of 2 and a maximum of 32 samples applied. For the estimation of specific gravity in the North domains, due to the paucity of data, values calculated from the regression technique where used in the estimation. For the Main domains, only measured density values were used, but the minimum number of samples used for the second and third search passes was reduced to 2. In all cases, a maximum of 5 samples per hole were used. Overall, 77% of the resource was estimated in the first pass. However, some more sparsely-sampled areas were predominantly estimated on the second or third pass. This has been taken into account during the resource classification. Un-estimated blocks, i.e. those outside the range of the third pass, were assigned the estimated domain mean and contribute less than 0.5% by volume to the resource. Hard boundaries were used between each of the four mineralisation domains. In the Main domains, estimation subdomains were utilised in order to align the search ellipse with the dominant orientation of the mineralisation. Between these subdomains, soft estimation boundaries were used. One-way estimation boundaries were used at the oxidation interface; i.e. oxidised and transitional material was estimated using both oxidised and fresh data, whereas the fresh domains used only fresh data.
	Any assumptions behind modelling of selective mining units.	No selective mining units were assumed in the estimate.
	Any assumptions about correlation between variables.	Strong positive correlation exists between nickel and all other elements estimated, with the exception of As (which has a weak positive correlation with nickel) and Mg (which has a moderate negative correlation with nickel). All elements within a domain used the same sample selection routine for block grade estimation.
	Description of how the geological interpretation was used to control the resource estimates.	The mineralisation interpretation was based on the 3D geological interpretation combined with grade data. Two grade domains, one at 0.5% Ni and the other at 1.0% Ni, were modelled for both the Main and North structures. The grade shells correlated well with the massive-semi-massive and disseminated units.
	Discussion of basis for using or not using grade cutting or capping.	Statistical analysis showed the populations in each domain at Camelwood to generally have a low coefficient of variation (CV) but it was noted that a very small number of outliers existed. No more than 2 samples per domain required top-cutting. Top cutting was not required for Mg or density.

Criteria	JORC Code explanation	Commentary
	The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.	Validation of the block model included a volumetric comparison of the resource wireframes to the block model volumes to within 0.5%. Validation of the estimate included comparing the block model grades to the declusted input data using a series of tables and swath plots showing north, easting and elevation comparisons. Visual validation of grade trends and metal distribution was also carried out. No mining has taken place, therefore no reconciliation data is available for comparison.
Moisture	Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.	The tonnages are estimated on a dry basis.
Cut-off parameters	The basis of the adopted cut-off grade(s) or quality parameters applied	A nominal grade cut-off of 0.5% Ni was used to define the mineralisation envelope. This correlates well with the geological logging of the disseminated and massive mineralisation and the barren host rock. Within the 0.5% Ni envelope a second domain representing material above 1.0% Ni was identified. This correlates with the massive and semi-massive material.
Mining factors or assumptions	Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.	No assumptions regarding the mining methodology have been built into the model; however, it is expected that mining of the Camelwood deposit will be dominantly by underground mining involving mechanised mining techniques.
Metallurgical factors or assumptions	The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	No assumptions regarding the metallurgical recovery have been built into the model.
Environmental factors or assumptions	Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made	No assumptions have been made regarding waste or process reside disposal. No issues are anticipated from an environmental perspective in the ultimate exploitation of the Mineral Resource, but these would be addressed in the next level of study.

Criteria	JORC Code explanation	Commentary
Bulk density	Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.	Bulk density was determined on diamond drill core by the assay laboratory using the water displacement method. A total of 197 out of 430 mineralised samples (before compositing) were missing density measurements. These were RC samples. Where no density data existed a regression formula was used to assign the density to be used in weighting of the data composites. The regression formula was generated from comparing nickel grades and density values for the Main domains only. The formula used is: SG_R = 0.1954 x Ni(%) + 2.81. Bulk density has been estimated from density measurements for the Main domains, and calculated regression density values for the North domains (due to the paucity of measured data within this domain). Estimated density values range from X t/m^3 to Y t/m^3.
	The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit,	The water displacement method adequately accounts for void spaces in the rock. Since the diamond drill core samples are fresh rock there are no moisture issues. The regression formula above used for the RC samples would account for any moisture, so sensitivity to these issues is considered low.
	Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.	See notes above.
Classification	The basis for the classification of the Mineral Resources into varying confidence categories	The Mineral Resource at Camelwood has been classified as Indicated and Inferred. The Indicated Resource is based on a nominal 50 m by 50 m to 75 m by 75 m spaced drill pattern, along with good confidence in the geological (volume) and grade continuity of the mineralisation. Areas where the drill spacing is greater than 75 m by 75 m have been classified as Inferred and exhibit lower confidence in the estimate of grade, specific gravity and volume of the mineralisation.
	Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).	Validation of the block model shows acceptable correlation of the input data to the estimated grades. The input data is comprehensive and no biases are believed to have been introduced. The geological model has a high degree of continuity and confidence. Infill drilling has confirmed this continuity.
	Whether the result appropriately reflects the Competent Person's view of the deposit.	The Mineral Resource estimate appropriately reflects the view of the Competent Persons.
Audits or reviews	The results of any audits or reviews of Mineral Resource estimates.	This is the maiden Camelwood Mineral Resource estimate. The resource was reviewed by Optiro and Rox personnel. No external resource review has been completed.
	Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate	The relative accuracy of the Mineral Resource estimate is reflected in the reporting of the Mineral Resource as per the guidelines of the JORC Code (2012 Edition). See above note on the classification of the Mineral Resource into varying confidence categories.
	The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used	The statement relates to global estimates of tonnes and grade.
	These statements of relative accuracy and confidence of the estimate should be compared with production data, where available	No production is available.

Competent Person Statement:

The information in this report that relates to Exploration Results is based on information compiled by Mr Ian Mulholland BSc (Hons), MSc, FAusIMM, FAIG, FSEG, MAICD, who is a Fellow of The Australasian Institute of Mining and Metallurgy and a Fellow of the Australian Institute of Geoscientists. Mr Mulholland has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration, and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Mulholland is a full time employee and Managing Director of the Company and consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

The information in this report that relates to Mineral Resources is based on information compiled by Mr Mark Drabble B.App.Sci (Geology), MAusIMM, who is a Member of The Australasian Institute of Mining and Metallurgy. Mr Drabble has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration, and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Drabble is Principal Consultant Geologist – Optiro Pty Ltd, and consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

About Rox Resources

Rox Resources Limited is an emerging Australian minerals exploration company. The company has four key assets at various levels of development with exposure to gold, nickel, zinc, lead, copper and phosphate, including the Mt Fisher Gold Project (WA), Myrtle/Reward Zinc-Lead Project (NT), the Bonya Copper Project (NT) and the Marqua Phosphate Project (NT).

Mt Fisher Gold-Nickel Project (100% + Option to Purchase)

The Mt Fisher gold project is located in the highly prospective North Eastern Goldfields region of Western Australia and in addition to being well endowed with gold the project hosts a strong potential for nickel. The total project area is 655km^2, consisting of a 485km^2 area 100% owned by Rox and an Option to purchase 100% of a further 170km^2.

Recent drilling at the Camelwood nickel prospect has intersected **semi-massive to massive and disseminated nickel sulphide mineralisation** in a number of holes along an 1,200m strike length and up to 500m depth, including **11.4m @ 2.9% Ni** and **6.2m @ 3.3% Ni**, with the mineralisation open in all directions.

Drilling by Rox has also defined numerous high-grade gold targets and a Measured, Indicated and Inferred Mineral Resource of **973,000 tonnes grading 2.75 g/t gold** exists for 86,000 ounces of gold (Measured: 171,900 tonnes grading 4.11 g/t Au, Indicated: 204,900 tonnes grading 2.82 g/t Au, Inferred: 596,200 tonnes grading 2.34 g/t Au).

Reward Zinc-Lead Project (Farm-out Agreement)

Rox has signed an Earn-In and Joint Venture Agreement with Teck Australia Pty Ltd. ("Teck") to explore its 670km^2 Myrtle/Reward zinc-lead tenements, located 700km south-east of Darwin, Northern Territory.

The Myrtle deposit has a current JORC Inferred Mineral Resource of **43.6 Mt @ 5.04% Zn+Pb** (Indicated: 5.8 Mt @ 3.56% Zn, 0.90% Pb; Inferred: 37.8 Mt @ 4.17% Zn, 0.95% Pb).

Recent drilling at the Teena prospect intersected **26.4m @ 13.3% Zn+Pb,** including **16.2m @ 17.2% Zn+Pb, and 20.1m @ 15.0% Zn+Pb,** including **12.5m @19.5% Zn+Pb**. Under the terms of the Agreement, Teck has now met the expenditure requirement for a 51% interest. Teck has elected to increase its interest in the project to 70% by spending an additional A$10m (A$15m in total) by 31 August 2018.

Bonya Copper Project (Farm-in Agreement to earn up to 70%)

In October 2012 Rox signed a Farm-in Agreement with Arafura Resources Limited to explore the Bonya Copper Project located 350km east of Alice Springs, Northern Territory. Outcrops of visible copper grading up to 34% Cu and 27 g/t Ag are present. Under the agreement, Rox can earn a 51% interest in the copper, lead, zinc, silver, gold, bismuth and PGE mineral rights by spending $500,000 within the first two years. Rox can elect to earn a further 19% (for 70% in total) by spending a further $1 million over a further two years. Once Rox has earned either a 51% or 70% interest it can form a joint venture with Arafura to further explore and develop the area.

Marqua Phosphate Project (100%)

Rox owns one tenement covering approximately 660 km^2 in the Northern Territory which comprises the Marqua Phosphate project. The project has the potential for a sizeable phosphate resource to be present, with surface sampling returning values up to 39.4% P_2O_5 and drilling (including 6m @ 19.9% P_2O_5 and 5m @ 23.7% P_2O_5) confirming a 30km strike length of phosphate bearing rocks.