

INVESTMENT HIGHLIGHTS

- Developing a large scale coking coal basin
- Two exceptionally well located coking coal deposits
- Combined Resources of 536.3 Mt
- Amaam North:
 - Project F: 72.3 Mt total Resource comprising 12.6Mt Measured^D, 13.2Mt Indicated^C & 46.6Mt Inferred^B
 - Outstanding exploration upside for resource growth
 - Project 35km from TIG's owned and operated Beringovsky coal port
 - PFS completed
 - BFS due for completion in Q4 2014
 - Short timeline to first production from low capital and operating cost mine

Amaam:

- Amaam: 464 Mt total Resource comprising 78Mt Indicated^C & 386Mt Inferred^B
- Project 25km from planned port site and only 8 days shipping to China, Korea and Japan
- High vitrinite content (>90%) coking coal with excellent coking properties
- PFS completed on 6.5Mtpa coking coal mine

BOARD OF DIRECTORS

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CHIEF EXECUTIVE OFFICER Craig Parry

Tigers Realm Coal Limited
ACN 146 752 561 ASX code: "TIG"
Level 7, 333 Collins St, Melbourne VIC 3000
T: (+61) 3 8644 1326

TIGERS REALM COAL INCREASES AMAAM NORTH COKING COAL RESOURCE BY 170%

Highlights:

- Updated JORC compliant Resource of 72.3Mt defined for Amaam North comprising 12.6Mt Measured^D, 13.2Mt Indicated^C and 46.6Mt Inferred^B
- Resource base increased by 170% (45.5Mt) since July 2013
- Measured and Indicated resources increased by nearly 120% from 11.8Mt to 25.8Mt
- Increased Resources incorporate Project F and its Eastern and Southern extensions. Majority of the Amaam North Licence remains undrilled.
- Updated Resource provides potential to increase mine life and production rates and further enhance the excellent economics of Project F
- Work continues on the Project F Bankable Feasibility Study (BFS) which will be completed in Q4 2014

Tigers Realm Coal Limited (ASX: TIG) is pleased to report an updated coking coal Resource of 72.3Mt at Project F, the first of several areas to be tested on the highly prospective Amaam North licence block (Figure 1), located in the Chukotka Province of far eastern Russia.

TIG completed the first major drilling campaign at Project F at Amaam North which was targeted due to the presence of thick, shallow-dipping coking coal seams outcropping only 18km from an existing road and 35km from the Company's operating coal port at Beringovsky, on the Pacific coast. Drilling through the 2013/14 winter season resulted in discovery of large strike extensions of the seams, substantially increasing total Resource tonnages and further increasing the tonnages in Measured and Indicated categories by nearly 120%.

Amaam Coking Coal Project

Tigers Realm Coal (TIG) owns 80%^A of the Amaam Coking Coal Project which is located in the Chukotka Province of far eastern Russia. The Amaam Coking Coal Project consists of two tenements: Amaam and Amaam North.

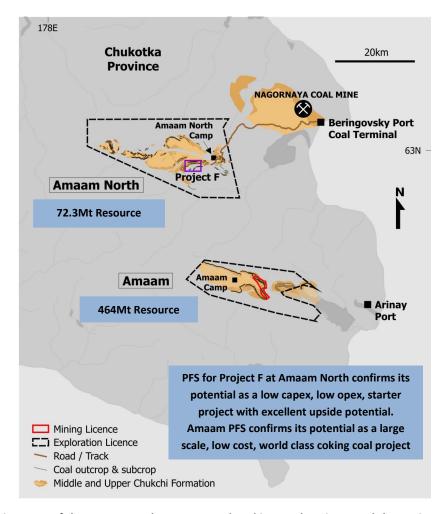


Figure 1. Location map of the Amaam and Amaam North Coking Coal Projects and the Project F Development

Amaam North, Deposit F Resource Estimate^B

Resource consultant Resolve Geo Pty Ltd has estimated 72.3Mt of Coal Resources at Deposit F in the Amaam North licence block. This includes Measured Resources of 12.6Mt, Indicated Resources of 13.2Mt and Inferred Resources of 46.6Mt.

About 58.6Mt of the total Coal Resource is in the open pit domain less than 150m from surface. Below 150m, the Resource holds a further 13.7 Mt, providing significant potential upside for underground operations.

The Resource estimate is based on 116 drill holes totalling 9698m, outcrop mapping and sampling, and structural interpretations of satellite photography and Landsat imagery.

The following tables detail the Deposit F Resource Estimate. Totals below may not sum due to rounding.

Coal Resources for the Amaam North - Project F (100% basis)

Resource Category	Open Pit ¹ (Mt)	Underground ² (Mt)	Total (Mt)
Measured - Coking	12.6	0	12.6
Indicated- Coking	7.7	3.9	11.5
Inferred - Coking	33.2	9.9	43.1
Indicated - Thermal	1.7	0	1.7
Inferred - Thermal	3.5	0	3.5
Total	58.6	13.7	72.3

By Depth	Coking (Mt)	Thermal (Mt)	Total (Mt)
Surface to 50m	15.5	5.2	20.7
50 to 100m	20.1	-	20.1
100 to 150m	17.8	-	17.8
Greater than 150m	13.7	-	13.7
Total	67.2	5.2	72.3

Coal Quality by Depth (air dried basis)

	Open Pit ¹	Underground ²	Total
In Situ Tonnes (Mt)	58.6	13.7	72.3
In-Situ Density (ISD) g/cm3	1.42	1.40	1.42
Air dried moisture (ADM) %ad	1.2	1.4	1.2
Ash %ad	17.9	15.5	17.5
Volatile Matter (VM) %ad	26.0	26.9	26.2
Fixed Carbon(FC) %ad	54.9	56.3	55.1
Sulphur (S) %ad	0.32	0.28	0.31
Calorific value (CV) kcal/kg ad	6633	6883	6697

Coal Quality by Ply (air dried basis)

Ply	Mt	ISD	ADM	Ash	VM	FC	S	CV
422	5.1	1.39	1.2	14.1	27.3	57.4	0.83	7019
421	2.9	1.38	1.1	13.5	26.7	58.7	0.40	7038
402	0.6	1.53	1.3	29.4	23.9	45.4	0.28	5549
41	24.3	1.38	1.3	13.9	27.5	57.4	0.29	6953
35	5.0	1.50	1.1	25.1	24.5	49.3	0.26	5974
34	1.6	1.47	1.1	26.9	24.5	47.5	0.24	5785
33	0.4	1.56	1.2	32.1	24.9	41.9	0.18	5233
32	2.9	1.47	1.1	21.4	25.9	51.5	0.20	6343
31	3.2	1.42	1.1	17.3	26.5	55.0	0.22	6729
22	1.0	1.47	1.1	21.3	24.4	53.2	0.24	6316
21	4.4	1.44	1.2	18.1	24.2	56.6	0.24	6658
12	3.6	1.47	1.2	20.2	23.0	55.7	0.26	6425
11	1.8	1.57	1.1	31.9	21.5	45.4	0.23	5279
5	1.8	1.49	1.6	30.4	23.1	44.9	0.27	6008
WS4 ³	13.7	1.40	1.4	15.5	26.9	56.3	0.28	6883
Total	72.3	1.42	1.26	17.6	26.1	55.0	0.31	6697

- 1. Assumes coal seams greater 0.3m to a depth of 150m
- 2. Assumes coal seams greater than 1.2m deeper than 150m
- 3. Underground working section

The following figures illustrate the Project F coal geology and Resources. Figure 2 shows on plan the extent of drilling, and cumulative coal thickness.

Figure 3 shows the typical extents of Measured, Indicated and Inferred Resources (Seam 41 Resource polygon extent illustrated). Individual seams vary according to inclusion criteria defined by core recovery. Lower seams also show thinning and deterioration from east to west (refer to the cross section in Figure 4). The deposit comprises shallow dipping coal seams over an 11km strike length. Inferred Resources in this Resource are projected from the sub-crop zone (i.e. in the down dip direction) for approximately 800-1600m or to where the deposit is limited down-dip by bounding faults, which are largely interpreted from topography and geological mapping, with some confirmation by drilling. To the east the Resources are limited by the tenement boundary, and to the south Resources are limited by strip ratio cut-off, as the seams become thin.

Figure 4 shows a longitudinal section through the deposit illustrating the seam correlations. The majority of the Resource tonnage is in seams with thicknesses greater than 1m. Seams of <30cm are not included within the Resource tonnages.

The deposit at Project F is comprised of mid to high-volatile bituminous coking coal. The upper coal seams (Plies 422, 421 and 41) comprise approximately 55% of the open pit deposit and have an average ash content of 13.9%, however within the Indicated and Measured resource footprint the ash is 11.1%. These seams will provide the majority of the bypass, low ash coking coal product (i.e. direct shipping coal) that will be targeted during operations. The lower seams have an average ash of 22.6% and will require washing to produce a coking coal product. Initial clean coal test results indicate that Project F product coals will have a Rank (RoMax) of 1.0 - 1.1 and a Free Swelling Index (FSI) between 6 and 7.

The near surface coals in the deposit are oxidised to the extent that their FSI values are low (less than 1), but they retain high calorific value. These coals have a modelled ash of 18.4% (air dried) and a modelled air dried calorific value of approximately 6,030 kcal/kg. These coals make up only a small component of the total Project F Resource, and TIG plans to market this coal to the domestic (Far East Russian) and Asian energy markets.

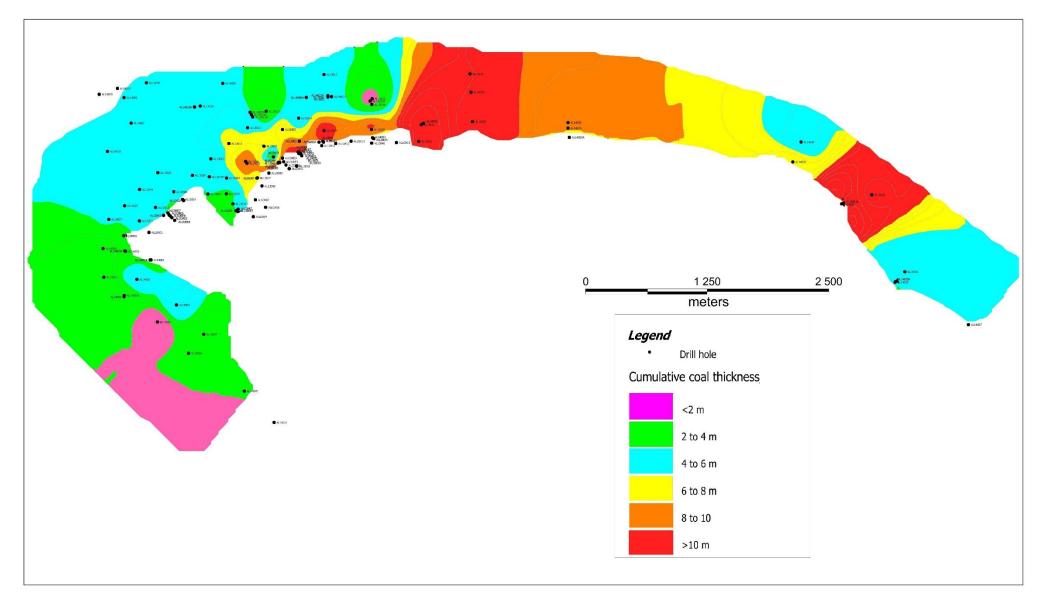


Figure 2. Plan showing drill hole locations and cumulative coal thicknesses

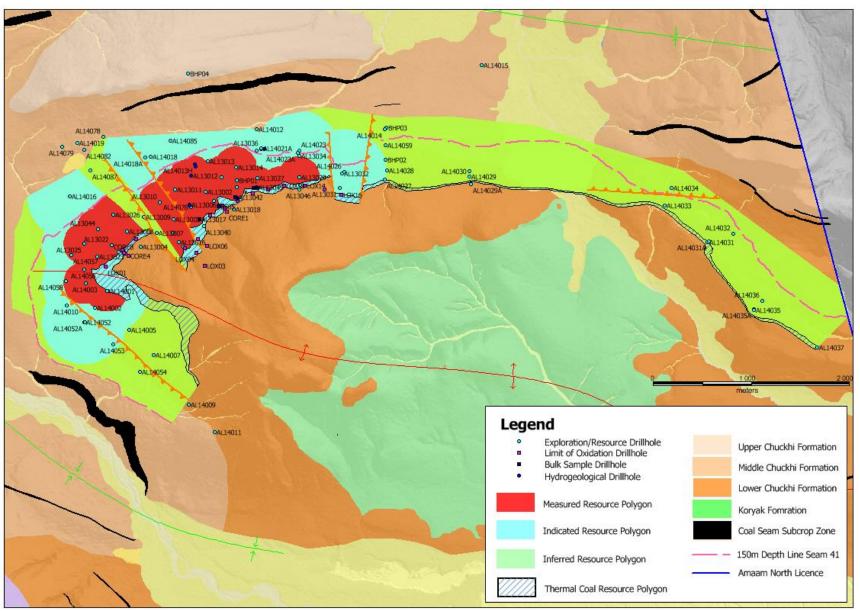


Figure 3. Amaam North Project F Resource Boundaries showing Measured, Indicated and Inferred Resources of 41 Seam (Note: Indicated and Measured Resource Polygons vary on a seam by seam basis according to core recovery and seam splitting character)

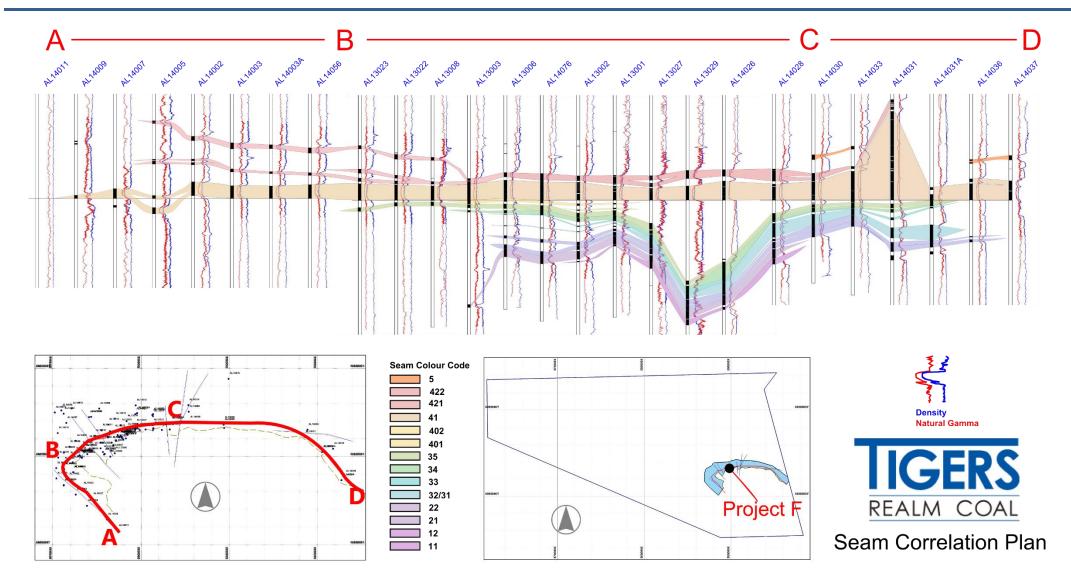


Figure 4. Amaam North Project F Resource Seam Correlation Plan

Total

155 to 480

Exploration Upside at Amaam North

The current Amaam North Exploration Target of 155 to 480Mt was announced in TIG's ASX release on 19 February 2014.

	Lower Chukchi Coal (Mt)	Middle Chukchi Coal (Mt)	Total (Mt)
Open Pit ¹	45 to 85	80 to 235	130 to 320
Underground ²	15 to 55	10 to 105	25 to 160

90 to 340

Amaam North Exploration Target^E

1. Assumes coal seams greater 0.3m to a depth of 250m

60 to 140

2. Assumes coal seams greater than 1.2m from 250m to 400m depth

TIG will follow up on prospective areas to the south and west of Project F (Figure 5). A re-interpretation of surface geology based on acquired Ikonos satellite photography and LandSat imagery, has indicated the potential for a much larger area of the Lower Chukchi formation (the Project F Coal Bearing Sediments) than previously thought.

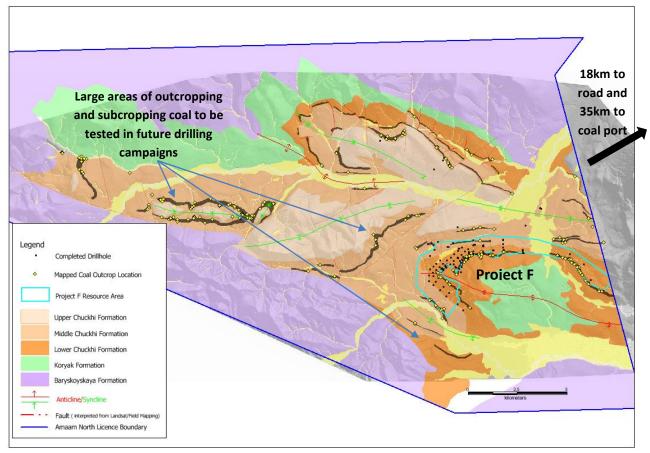


Figure 5. Amaam North Geology Map showing Project F and latest interpretation of Lower Chukchi Formation

Further details about Tigers Realm Coal can be found at www.tigersrealmcoal.com

For further information, contact:

Craig Parry - Chief Executive Officer +61 3 8644 1326

The information compiled in this report relating to resources is based on information compiled by Neil Biggs, who is a member of the Australian Institute of Mining and Metallurgy (AusIMM) and who is employed by Resolve Geo Pty Ltd. Neil has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity he is undertaking to qualify as a Competent Person as defined in the 2012 edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Neil Biggs consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

Signed

Neil Biggs

Date: 14 October 2014

About Tigers Realm Coal Limited (ASX: TIG)

Tigers Realm Coal Limited ("TIG", "Tigers Realm Coal" or "the Company") is an Australian based resources company. The Company's vision is to build a global coking coal company by rapidly advancing its projects through resource delineation, feasibility studies and mine development to establish profitable operations.

Competent Persons Statement

The information compiled in this announcement relating to exploration results, exploration targets or Coal Resources at Amaam and Amaam North is based on information provided by TIG and compiled by Neil Biggs, who is a member of the Australasian Institute of Mining and Metallurgy and who is employed by Resolve Coal Pty Ltd, and has sufficient experience which is relevant to the style of mineralization and type of deposit under consideration and to the activity he is undertaking to qualify as a Competent Person as defined in the JORC Code. Neil Biggs consents to the inclusion in the announcement of the matters based on his information in the form and context which it appears.

Note A - Tigers Realm Coal's interests in the Amaam Coking Coal Project

Amaam tenement: TIG's current beneficial ownership is 80%. TIG will fund all project expenditure until the completion of a bankable feasibility study each joint venture party is required to contribute to further project expenditure on a pro-rata basis. TIG's 20% partner, Siberian Tigers International Corporation, is also entitled to receive a royalty of 3% gross sales revenue from coal produced from within the Amaam licence.

Amaam North tenement: TIG has 80% beneficial ownership of the Russian company which owns the Amaam North exploration licence, Beringpromugol LLC. TIG will fund all project expenditure until the completion of a bankable feasibility study. After completion of a bankable feasibility study each joint venture party is required to contribute to further project expenditure on a pro-rata basis. BS Chukchi Investments LLC (BSCI) is also entitled to receive a royalty of 3% gross sales revenue from coal produced from within the Amaam North licence.

Note B - Inferred Resources

According to the commentary accompanying the JORC Code an 'Inferred Mineral Resource' is that part of a Mineral Resource for which quantity and grade (or quality) are estimated on the basis of limited geological evidence and sampling. Geological evidence is sufficient to imply but not verify geological and grade (or quality) continuity. It is based on exploration, sampling and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes. An Inferred Mineral Resource has a lower level of confidence than that applying to an Indicated Mineral Resource and must not be converted to an Ore Reserve. It is reasonably expected that the majority of Inferred Mineral Resources could be upgraded to Indicated Mineral Resources with continued exploration

Note C - Indicated Resources

According to the commentary accompanying the JORC Code an 'Indicated Mineral Resource' is that part of a Mineral Resource for which quantity, grade (or quality), densities, shape and physical characteristics are estimated with sufficient confidence to allow the application of modifying factors in sufficient detail to support mine planning and evaluation of the economic viability of the deposit. Geological evidence is derived from adequately detailed and reliable exploration, sampling and testing gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes, and is sufficient to assume geological and grade (or quality) continuity between points of observation where data and samples are gathered.

Note D – Measured Resources

According to the commentary accompanying the JORC Code a 'Measured Mineral Resource' is that part of a Mineral Resource for which quantity, grade (or quality), densities, shape, and physical characteristics are estimated with confidence sufficient to allow the application of Modifying Factors to support detailed mine planning and final evaluation of the economic viability of the deposit. Geological evidence is derived from detailed and reliable exploration, sampling and testing gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes, and is sufficient to confirm geological and grade (or quality) continuity between points of observation where data and samples are gathered. A Measured Mineral Resource has a higher level of confidence than that applying to either an Indicated Mineral Resource or an Inferred Mineral Resource. It may be converted to a Proved Ore Reserve or under certain circumstances to a Probable Ore Reserve.

Note E – Exploration Target

According to the commentary accompanying the JORC Code An Exploration Target is a statement or estimate of the exploration potential of a mineral deposit in a defined geological setting where the statement or estimate, quoted as a range of tonnes and a range of grade (or quality), relates to mineralisation for which there has been insufficient exploration to estimate a Mineral Resource. Any such information relating to an Exploration Target must be expressed so that it cannot be misrepresented or misconstrued as an estimate of a Mineral Resource or Ore Reserve. The terms Resource or Reserve must not be used in this context.

APPENDIX A – Summary Drilling Results Amaam North

Hole	Easting	Northing	RL	Total Depth	Base of Oxidation	Hole Type	Comments
AL13001	589600.98	6983266.03	139.63	58.60	19.96	HQ Core	
AL13002	589237.19	6983215.68	123.76	67.60	13.08	HQ Core	
AL13003	588857.18	6982889.85	126.04	91.20	23.17	HQ Core	
AL13004	588476.97	6982566.26	130.20	91.20	12.06	HQ Core	No coal
AL13005	589429.09	6983386.25	114.50	79.00	13.62	HQ Core	
AL13006	589051.07	6983059.05	121.97	61.00	12.53	HQ Core	
AL13007	588666.15	6982726.94	132.25	87.90	14.27	HQ Core	
AL13008	588317.20	6982749.00	109.66	64.00	11.44	HQ Core	
AL13009	588507.69	6982916.98	111.48	115.20	19.30	HQ Core	
AL13010	588696.56	6983086.04	110.56	109.00	13.88	HQ Core	
AL13011	588881.08	6983241.84	105.39	103.20	10.88	HQ Core	
AL13012	589071.08	6983403.95	102.33	118.30	22.88	HQ Core	
AL13013	589262.08	6983571.22	92.86	127.20	16.12	HQ Core	
AL13014	589593.14	6983500.66	105.12	70.00	16.29	HQ Core	
AL13016	588921.53	6982627.18	157.66	40.00	11.93	HQ Core	No coal
AL13017	589170.10	6982890.84	143.33	58.50	11.43	HQ Core	
AL13018	589572.36	6983011.95	166.19	34.50	25.96	HQ Core	No coal
AL13019	589336.13	6983104.97	143.03	61.10	20.95	HQ Core	
AL13022	588131.40	6982588.38	106.88	91.00	8.80	HQ Core	
AL13023	587966.62	6982452.49	103.81	55.20	7.42	HQ Core	
AL13024	588407.46	6982672.32	121.63	40.00	10.27	HQ Core	
AL13025	587815.05	6982606.72	91.34	85.30	11.37	HQ Core	
AL13026	588153.65	6982944.29	93.64	118.45	19.30	HQ Core	
AL13027	589851.84	6983374.40	133.98	67.30	16.00	HQ Core	
AL13029	590336.56	6983384.80	149.34	73.60	8.85	HQ Core	
AL13031	590818.80	6983264.10	156.39	69.20	24.03	HQ Core	
AL13032	590845.67	6983435.10	139.44	79.50	9.06	HQ Core	No coal
AL13034	590341.07	6983640.70	127.68	121.00	7.24	HQ Core	No coal
AL13036	589890.37	6983717.52	110.37	121.00	16.90	HQ Core	No coal
AL13039	588855.03	6982728.37	140.10	79.20	24.97	HQ Core	
AL13040	589217.35	6982808.24	152.86	37.50	19.41	HQ Core	
AL13041	589386.83	6983050.17	150.96	45.00	24.01	HQ Core	
AL13042	589600.43	6983150.93	152.07	37.50	16.42	HQ Core	
AL13043	588212.34	6982507.72	122.87	36.60	8.96	HQ Core	
AL13044	587967.80	6982772.79	89.19	93.90	6.45	HQ Core	
AL13045	589839.36	6983265.60	144.49	40.20	8.11	HQ Core	
AL13046	590338.07	6983245.57	161.01	82.50	14.75	HQ Core	No coal
AL13047	588974.09	6982571.00	165.67	52.50	22.66	HQ Core	
AL14012	589851.30	6983947.71	84.27	195.30	16.68	Open Hole	
AL14014	591343.87	6983953.71	87.30	120.40	12.89	Open Hole	
AL14016	587639.97	6983162.30	114.32	252.50	15.39	HQ Core	
AL14018	588587.68	6983624.77	117.62	93.10	15.89	HQ Core	No coal
AL14018A	588528.31	6983615.12	116.80	271.00	17.86	HQ Core	2 234.
AL14021	589842.94	6983698.34	0.00	211.00	13.41	HQ Core	
AL14021A	589890.81	6983730.13	109.87	222.00	17.37	HQ Core	
AL14022	590347.94	6983300.46	150.32	61.00	11.16	HQ Core	
AL14023	590345.47	6983699.88	124.03	42.80	5.25	HQ Core	No coal

Hole	Easting	Northing	RL	Total Depth	Base of Oxidation	Hole Type	Comments
AL14023A	590322.24	6983675.41	125.27	177.60	11.49	HQ Core	
AL14026	590867.98	6983449.46	139.60	160.00	9.32	HQ Core	
AL14026A	590867.98	6983449.46	139.60	145.00	9.64	HQ Core	No coal
AL14066	589590.74	6983151.82	149.10	29.00	14.92	HQ Core	
AL14070	589615.89	6983133.01	157.12	21.20	9.08	HQ Core	
AL14071	589604.98	6983143.53	150.31	25.00	8.50	HQ Core	
AL14076	589065.85	6983040.28	133.17	60.00	11.40	HQ Core	
AL14085	588817.69	6983857.26	99.15	70.00	9.10	HQ Core	
AL14087	587882.63	6983450.68	112.27	50.00	11.80	HQ Core	No coal
ALCORE1	589496.89	6982985.57	162.13	20.00	20.00	HQ Core	No coal
ALCORE2	589463.83	6983022.22	155.56	30.00	19.00	HQ Core	
ALCORE3	589439.52	6983055.78	151.36	35.00	17.70	HQ Core	
ALCORE4	588327.40	6982457.92	136.65	20.00	20.00	HQ Core	No coal
ALCORE5	588296.81	6982485.55	134.74	27.00	14.55	HQ Core	
ALCORE6	588267.59	6982514.34	130.43	37.00	13.00	HQ Core	
ALCORE7	588257.34	6982533.87	127.15	30.00	11.42	HQ Core	
ALCORE8	588281.03	6982501.66	130.16	20.00	20.00	HQ Core	
ALCORE9	589428.94	6983093.62	148.24	30.00	20.13	HQ Core	
ALLOX01	588064.74	6982333.88	116.05	25.00	8.15	HQ Core	
ALLOX02	588417.76	6982660.34	126.57	23.00	12.18	HQ Core	
ALLOX04	589129.14	6982494.89	186.52	36.00	36.00	HQ Core	No coal
ALLOX05	588953.39	6982555.58	172.57	55.00	36.00	HQ Core	
ALLOX06	589255.54	6982590.60	188.86	31.00	31.00	HQ Core	
ALLOX07	589151.35	6982666.74	165.97	37.17	37.00	HQ Core	
ALLOX09	589289.19	6982940.76	143.04	31.00	14.69	HQ Core	
ALLOX10	589624.90	6983116.63	156.42	28.00	10.56	HQ Core	
ALLOX11	589828.81	6983220.80	150.84	22.00	15.77	HQ Core	
ALLOX12	589971.12	6983241.96	153.64	24.00	19.25	HQ Core	No coal
ALLOX13	590128.89	6983265.43	158.71	27.00	25.40	HQ Core	
ALLOX14	590359.42	6983292.04	157.61	27.00	16.57	HQ Core	
ALLOX15	590591.59	6983252.56	153.46	31.00	7.30	HQ Core	No coal

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Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
AL13001	35.14	36.62	1.48	42	✓	✓	✓
AL13001	36.94	39.3	2.36	41	✓	✓	✓
AL13001	39.73	39.94	0.21	402	✓	✓	✓
AL13001	40.54	40.72	0.18	401	✓	<u> </u>	✓
AL13001	41.26	41.81	0.55	35	✓	<u> </u>	✓
AL13001	42.08	42.41	0.33	34	✓	<u>√</u>	✓
AL13001	43.09	43.24	0.15	32	✓	<u>√</u>	*
AL13001	44.01	44.46	0.45	22	✓	<u>√</u>	√
AL13001	44.48	45.07	0.59	21	✓	<u>√</u>	√
AL13001	45.18	46.58	1.4	12	✓	<u>√</u>	✓
AL13001	46.86	47.05	0.19	11	✓	✓	*
AL13002	36.06	36.1	0.04	5	✓	*	
AL13002	40.97	41.79	0.82	42	√	<u>√</u>	*
AL13002	43.52	45.01	1.49	41	✓	<u>√</u>	*
AL13002	45.56	45.91	0.35	402	√	<u>√</u>	√
AL13002	46.55	46.7	0.15	401	✓	<u> </u>	√
AL13002	47.08	47.92	0.84	35	✓	<u> </u>	∀
AL13002	47.99	48.51	0.52	34	✓	<u>√</u>	V
AL13002	49.18	49.31	0.13	33	√	√	Y
AL13002	50.09	50.23	0.14	32	√	<u>*</u>	/
AL13002	51.84	52.3	0.46	22	*		✓
AL13002	52.38	53.19	0.81	21	√	<u>√</u>	Ť
AL13002	53.33	54.49	1.16	12	✓	<u> </u>	✓
AL13002	55	55.15	0.15	11	·		
AL13003	58.52	59.22	0.7	421	√	<u> </u>	√
AL13003	59.22	62.08	2.86	41	∀	<u> </u>	V
AL13003	62.08	62.66	0.58	402	∀	<u> </u>	V
AL13003	62.79	63.37	0.58	35	∀	<u> </u>	V
AL13003	63.73	64.04	0.31	34	∀	<u> </u>	•
AL13003	79.27	79.74	0.47	12	∀	<u> </u>	*
AL13005	51.54	52.43	0.89	42	∀	<u> </u>	▼
AL13005	52.43	54.04 55.31	1.61	41	∀	<u> </u>	▼
AL13005	55 55.76	56.28	0.31 0.52	40	→	<u> </u>	· /
AL13005 AL13005	56.48	56.28	0.52	35 34	· /	*	•
AL13005 AL13005	58.54	58.95	0.42	32	· · · · · · · · · · · · · · · · · · ·	<u>~</u> ✓	✓
AL13005 AL13005	59.46	59.54	0.41	31	→	*	•
AL13005 AL13005	60.38	60.85	0.08	22	→	<u>~</u> ✓	✓
AL13005 AL13005	60.9	61.82	0.47	21	· · · · · · · · · · · · · · · · · · ·	<u> </u>	·
AL13005 AL13005	61.88	63	1.12	12	· ·	<u> </u>	· /
AL13005	63	63.49	0.49	11	· ✓	<u> </u>	· ·
AL13005	38.41	40.04	1.63	42	✓	<u> </u>	<i>✓</i>
AL13006	40.24	42.99	2.75	41	· ✓	<u> </u>	√
AL13006	43.11	43.23	0.12	402	<i>√</i>	<u> </u>	√
AL13006	43.34	43.45	0.11	401	✓	<u>·</u>	×
AL13006	43.64	44.38	0.74	35	✓	✓	✓
AL13006	44.66	45.08	0.42	34	✓	✓	✓
AL13006	45.2	45.31	0.11	33	✓	✓	✓
AL13006	47.17	47.28	0.11	32	✓	✓	✓
AL13006	48.82	49.26	0.44	22	✓	✓	✓
AL13006	50.28	50.97	0.69	21	✓	✓	✓
AL13006	50.97	52.27	1.3	12	✓	✓	✓
AL13008	35.99	36.46	0.47	422	✓	✓	✓
AL13008	40.02	40.41	0.39	421	✓	✓	✓
AL13008	40.64	43.06	2.42	41	✓	✓	✓
AL13008	43.36	43.99	0.63	35	✓	✓	─
AL13010	82.11	82.79	0.68	421	✓	✓	✓
AL13010	82.79	85.37	2.58	41	✓	✓	✓
AL13010	85.51	85.77	0.26	402	✓	✓	×
AL13010	86.71	87.19	0.48	35	✓	✓	✓
AL13010	87.66	87.95	0.29	34	✓	✓	×
AL13010	99.77	100.33	0.56	12	✓	sc .	
AL13011	67.44	68.99	1.55	42	✓	✓	✓
							2 12 of 20

Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
AL13011	69.27	71.36	2.09	41	✓	✓	✓
AL13011	72.16	72.41	0.25	402	✓	✓	✓
AL13011	73.09	73.12	0.03	401	✓	*	
AL13011	74.71	75.36	0.65	35	✓	<u>√</u>	√
AL13011	75.62	76.07	0.45	34	✓	√	✓
AL13011	78.05	78.12	0.07	32	✓	<u> </u>	
AL13011	80.12	80.41	0.29	22	√	<u> </u>	∀
AL13011	86.5	87.19	0.69	12	√	<u>√</u>	∀
AL13012	87.66	89.07	1.41	42	▼	<u> </u>	· · ·
AL13012	89.49	91.72	2.23	41 402	→	<u> </u>	√
AL13012 AL13012	92.98 96.3	93.18 96.43	0.2 0.13	402	· · · · · · · · · · · · · · · · · · ·		•
AL13012 AL13012	98.8	99.4	0.13	34	· · · · · · · · · · · · · · · · · · ·	<u> </u>	✓
AL13012	102.18	102.41	0.23	31	· ✓	<u>·</u>	√
AL13012	104	104.21	0.21	22	✓	<u> </u>	✓
AL13012	107.32	108.22	0.9	12	✓	✓	✓
AL13013	114.52	115.53	1.01	42	✓	✓	×
AL13013	116.58	118.02	1.44	41	✓	✓	✓
AL13014	47.02	48.94	1.92	42	✓	✓	✓
AL13014	51.1	53.67	2.57	41	✓	✓	✓
AL13017	13.95	15.34	1.39	42	✓	✓	✓
AL13017	15.45	18.15	2.7	41	✓	✓	✓
AL13017	18.15	19.08	0.93	35	✓	✓	✓
AL13017	19.48	20.02	0.54	34	✓	✓	✓
AL13017	24.44	24.86	0.42	22	✓	✓	✓
AL13017	29.2	29.23	0.03	21	✓	*	
AL13017	29.6	31.03	1.43	12	✓	<u>√</u>	✓
AL13019	22.95	23.11	0.16	5	✓	√	✓
AL13019	26.65	27.82	1.17	42	✓	*	
AL13022	28.57	29.31	0.74	422	√	<u>√</u>	√
AL13022	32.43	32.66	0.23	4212	∀	<u> </u>	∀
AL13022	32.96	33.39	0.43	4211	∀	<u> </u>	∀
AL13022	33.68 36.5	36.07 37.05	2.39 0.55	41 35	▼	<u> </u>	▼
AL13022 AL13023	22.58	23.17	0.59	5	· · · · · · · · · · · · · · · · · · ·	<u> </u>	✓
AL13023 AL13023	26.45	27.17	0.72	422	· · · · · · · · · · · · · · · · · · ·	<u> </u>	· /
AL13023	27.99	28.48	0.72	421	· ✓	<u> </u>	· ·
AL13023	28.99	31.6	2.61	41	✓	<u> </u>	✓
AL13023	32.92	33.44	0.52	35	✓	x	
AL13024	11.01	11.67	0.66	421	✓	✓	✓
AL13024	11.67	14.41	2.74	41	✓	✓	✓
AL13024	14.58	15.26	0.68	35	✓	✓	✓
AL13025	55.32	55.43	0.11	5	✓	sc	
AL13025	59.74	60.62	0.88	422	✓	✓	✓
AL13025	63.07	63.49	0.42	421	✓	✓	✓
AL13025	64.09	66.4	2.31	41	√	✓	✓
AL13025	67.84	68.39	0.55	40	✓	x	
AL13026	78.99	79.19	0.2	5	✓	<u>√</u>	✓
AL13026	85.13	85.45	0.32	422	✓	<u> </u>	√
AL13026	88.68	89.18	0.5	421	✓	<u> </u>	√
AL13026	89.8	92	2.2	41	√	<u>√</u>	√
AL13026	92.53	93.03	0.5	35	√	√	✓
AL13027	36.65	37.6	0.95	422	√	<u>*</u>	
AL13027	37.89	38.71	0.82	421	∀	<u> </u>	x ✓
AL13027	38.83 44.87	40.9	2.07	41 35	∀	<u> </u>	*
AL13027	44.87	45.58 46.36	0.71 0.48	35 34	→	<u> </u>	~
AL13027 AL13027	45.88	46.36	0.48	33	→	<u> </u>	→
AL13027 AL13027	47.03	47.03	0.34	32	✓	<u> </u>	→
AL13027 AL13027	47.03	47.42	0.58	31	✓	<u> </u>	✓
AL13027 AL13027	48.05	48.76	0.71	22	✓	<u> </u>	√
AL13027 AL13027	48.84	49.79	0.71	21	√	<u> </u>	√
AL13027	49.79	51.1	1.31	12	✓	✓	✓
	.5.,5	~ ±.±	1.01				2 1 4 of 20

Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
AL13027	51.1	52.1	1	11	✓	✓	✓
AL13029	28.45	29.88	1.43	42	✓	✓	✓
AL13029	30.99	33.38	2.39	41	✓	✓	✓
AL13029	46.67	47.04	0.37	35	✓	✓	×
AL13029	47.49	48.03	0.54	34	✓	✓	✓
AL13029	48.03	48.78	0.75	33	✓	✓	✓
AL13029	48.78	49.17	0.39	32	✓	✓	✓
AL13029	49.17	49.57	0.4	31	✓	✓	✓
AL13029	49.57	50.5	0.93	22	✓	<u> </u>	✓
AL13029	50.5	51.8	1.3	21	✓	<u> </u>	✓
AL13029	51.8	52.9	1.1	12	✓	<u> </u>	✓
AL13029	52.98	53.94	0.96	11	✓	<u> </u>	✓
AL13031	37.93	40.66	2.73	41	✓	<u>√</u>	✓
AL13031	41.53	41.7	0.17	402	√	√	✓
AL13031	42.56	43.45	0.89	35	✓	<u> </u>	✓
AL13031	43.45	44.34	0.89	34	✓	<u> </u>	✓
AL13031	44.34	45.29	0.95	33	✓	✓	✓
AL13031	45.29	46.24	0.95	32	✓	✓	✓
AL13031	46.24	47.24	1	31	✓	✓	✓
AL13031	47.24	48.22	0.98	22	✓	✓	✓
AL13031	48.22	50.21	1.99	21	✓	√	✓
AL13031	50.21	51.77	1.56	12	✓	✓	✓
AL13031	51.77	53.17	1.4	11	✓	✓	✓
AL13039	55.67	58.08	2.41	41	✓	✓	✓
AL13039	58.08	59.04	0.96	35	✓	✓	✓
AL13039	59.42	59.75	0.33	34	✓	✓	✓
AL13040	4.08	5.3	1.22	42	✓	✓	✓
AL13040	5.3	8.08	2.78	41	✓	✓	✓
AL13040	8.08	9.09	1.01	35	✓	✓	✓
AL13040	9.25	9.85	0.6	34	✓	✓	✓
AL13040	13.35	13.4	0.05	22	✓	*	
AL13040	24.07	25.19	1.12	12	✓	✓	✓
AL13041	14.93	15.06	0.13	5	✓	<u> </u>	✓
AL13041	21	22.84	1.84	42	✓	<u> </u>	✓
AL13041	22.84	25.1	2.26	41	√	<u>√</u>	✓
AL13041	25.1	25.57	0.47	402	✓	<u>√</u>	√
AL13041	25.72	25.9	0.18	401	✓	<u>√</u>	√
AL13041	26	26.81	0.81	35	✓	<u> </u>	✓
AL13041	26.81	27.39	0.58	34	✓	√	✓
AL13041	29.3	29.43	0.13	32	V	<u> </u>	✓
AL13041	29.94	30.1	0.16	31	✓	<u>√</u>	√
AL13041	30.91	31.38	0.47	22	✓	√	✓
AL13041	31.49	32.53	1.04	21	✓	<u>√</u>	√
AL13041	32.69	33.53	0.84	12	√	<u> </u>	√
AL13042	10.26	11.89	1.63	42	✓	<u> </u>	√
AL13042	11.99	14.81	2.82	41	√	<u>√</u>	✓
AL13042	14.91	15.53	0.62	402	√	<u>√</u>	√
AL13042	15.61	15.84	0.23	401	√	<u> </u>	√
AL13042	15.93	16.61	0.68	35	√	<u> </u>	√
AL13042	16.67	17.48	0.81	34	✓	<u> </u>	√
AL13042	17.61	17.74	0.13	33	✓	<u> </u>	√
AL13042	18.05	18.29	0.24	32	√	<u> </u>	√
AL13042	18.36	18.75	0.39	31	✓	<u> </u>	√
AL13042	18.8	19.16	0.36	22	√	<u> </u>	√
AL13042	19.23	20.17	0.94	21	√	<u> </u>	√
AL13042	20.47	21.31	0.84	12	√	<u> </u>	V
AL13042	21.31	22.16	0.85	11	✓	<u> </u>	√
AL13043	12.43	13.28	0.85	422	√	<u>√</u>	√
AL13043	15.83	16.42	0.59	421	√	√	√
AL13043	16.8	19.21	2.41	41	√	√	√
AL13043	19.6	20.16	0.56	35	✓	<u> </u>	√
AL13044	63.34	63.56	0.22	5	√	<u> </u>	√
AL13044	68.29	69.01	0.72	422	✓	▼	• 15 of 20

Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
AL13044	71.68	72.19	0.51	421	✓	✓	✓
AL13044	72.44	75	2.56	41	✓	✓	✓
AL13044	75.78	76.17	0.39	40	✓	✓	✓
AL13045	4.1	6.89	2.79	42	✓	√	✓
AL13045	7.12	9.96	2.84	41	✓	<u>√</u>	✓
AL13045	11.05	11.21	0.16	402	√	<u>√</u>	√
AL13045	11.98	12.31	0.33	401	√	<u>√</u>	√
AL13045	12.57	13.45	0.88	35	√	<u>√</u>	√
AL13045	13.62	14.32	0.7	34	∀	<u>√</u>	√
AL13045	14.48	14.61	0.13	33	∀	<u> </u>	· · · · · · · · · · · · · · · · · · ·
AL13045	14.86	15.1	0.24	32	→	<u> </u>	•
AL13045 AL13045	15.49 15.96	15.65 16.4	0.16 0.44	31 22	→	<u> </u>	· ·
AL13045 AL13045	16.4	17.56	1.16	21	→	<u> </u>	
AL13045 AL13045	17.56	18.64	1.18	12	· ✓	<u> </u>	· /
AL13045	18.64	19.19	0.55	11	· ✓	<u> </u>	· ·
AL13043	31.67	32.54	0.87	421	· ✓	<u> </u>	· ✓
AL13047	32.91	35.98	3.07	41	✓	✓	✓
AL13047	35.98	36.6	0.62	402	· ✓	<u> </u>	✓
AL13047	36.6	37.55	0.95	35	✓	✓	✓
AL13047	38.01	38.46	0.45	34	✓	✓	*
AL14001	8.16	9.06	0.9	422	✓	✓	✓
AL14001	12.05	12.21	0.16	4212	✓	✓	✓
AL14001	12.38	12.79	0.41	4211	✓	✓	✓
AL14001	14.27	16.55	2.28	41	✓	✓	✓
AL14001A	9.47	10.44	0.97	422	✓	*	
AL14001A	13.44	13.57	0.13	4212	✓	*	
AL14001A	13.74	14.14	0.4	4211	✓	*	
AL14001A	15.7	17.91	2.21	41	✓	3 0	
AL14002	49.93	50.65	0.72	422	✓	.	
AL14002	53.44	53.72	0.28	4212	✓	*	
AL14002	53.98	54.32	0.34	4211	√	*	
AL14002	56.97	59.54	2.57	41	∀	<u> </u>	
AL14002	78.11	78.96	0.85	35	· · · · · · · · · · · · · · · · · · ·	*	
AL14002	79.17	79.71 30.73	0.54 0.92	34 422	∀	<u>~</u> ✓	*
AL14003 AL14003	29.81 33.85	34.33	0.92	422	,	<u> </u>	<u>~</u>
AL14003 AL14003	36.42	38.38	1.96	421	· ·	<u> </u>	· /
AL14003A	30.42	30.72	0.53	422	· ✓	3c	
AL14003A	34.33	34.56	0.23	421	✓	x	
AL14003A	36.54	38.44	1.9	41	✓	×	
AL14005	63.65	64.12	0.47	422	✓	3 0	
AL14005	69.59	70.35	0.76	421	✓	je.	
AL14005	75.19	75.64	0.45	412	✓	sc	
AL14005	76.98	78.2	1.22	411	✓	x	
AL14005	78.37	78.7	0.33	402	✓	x	
AL14005	78.96	79.28	0.32	401	✓	x	
AL14005	103.5	103.96	0.46	35	✓	3 0	
AL14005	104.47	105.39	0.92	34	✓	*	
AL14007	87.6	88.95	1.35	41	✓	.	
AL14007	89.95	90.31	0.36	402	√	*	
AL14007	90.97	91.36	0.39	401	√	*	
AL14009	44.61	45.15	0.54	421	√	*	
AL14009	53.11	53.5	0.39	412	√	3 5	
AL14009	53.73	54.3	0.57	411	∀	se se	
AL14010	38.14	38.83	0.69	422	∀	*	
AL14010	40.73	41.05	0.32	4212	∀	*	
AL14010 AL14010	45.53 48.61	45.83 49.24	0.3 0.63	4211 41	→	*	
AL14010 AL14010	48.61	49.24 49.64	0.63	402	→	*	
AL14010 AL14010	49.24	49.64	0.4	402	→	*	
AL14010 AL14016	217.2	217.41	0.21	<u>401</u> 5	→	*	
AL14016 AL14016	220.89	217.41	0.21	42	,	<u>~</u> ✓	✓
WF14010	220.09	441.00	0.90	42	*		16 of 20

AL14016 221.97 223.94 1.97 41 ✓ ✓ AL14016 223.94 224.17 0.23 402 ✓ ✓ AL14016 224.17 224.41 0.24 401 ✓ ✓ AL14016 226.25 226.39 0.14 33 ✓ ✓ AL14016 227.32 227.42 0.1 32 ✓ ✓ AL14018A 222.38 223.23 0.85 42 ✓ * AL14018A 226.72 228.7 1.98 41 ✓ *	√ √ √ √
AL14016 224.17 224.41 0.24 401 ✓ AL14016 226.25 226.39 0.14 33 ✓ AL14016 227.32 227.42 0.1 32 ✓ AL14018A 222.38 223.23 0.85 42 ✓ AL14018A 226.72 228.7 1.98 41 ✓	√
AL14016 226.25 226.39 0.14 33 ✓ AL14016 227.32 227.42 0.1 32 ✓ AL14018A 222.38 223.23 0.85 42 ✓ AL14018A 226.72 228.7 1.98 41 ✓	✓
AL14016 227.32 227.42 0.1 32 ✓ AL14018A 222.38 223.23 0.85 42 ✓ AL14018A 226.72 228.7 1.98 41 ✓	<u> </u>
AL14018A 222.38 223.23 0.85 42 ✓ ✗ AL14018A 226.72 228.7 1.98 41 ✓ ✗	✓
AL14018A 226.72 228.7 1.98 41 **	
ALI-010A 220.72 220.7 1.50 41	
AI 14018A	
AL14018A 235.94 236.73 0.79 35 ✓ AL14018A 252.29 252.97 0.68 12 ✓	
AL14019 88.06 99.01 10.95 422 *	
AL14019 99.01 101.58 2.57 421 *	
AL14019 102.25 104.16 1.91 41 ✓ *	
AL14019 106.82 107.36 0.54 40 ✓ *	
AL14019 127.58 130.23 2.65 22 *	
AL14019 130.23 132.53 2.3 21 🗸	
AL14019 132.75 133.39 0.64 1	
AL14021 165.51 166.68 1.17 41 ✓	*
AL14021 169.76 170.4 0.64 402 🗸	✓
AL14021 170.96 171.69 0.73 401 🗸	
AL14021 185.36 186.65 1.29 35 ✓	*
AL14021 187.17 187.71 0.54 34 ✓	*
AL14021 193.58 193.83 0.25 2	<u> </u>
AL14021 133.1 133.3 0.2 1	Y
76140217 100:02 107:71 1:03 41	
AL14021A 191 191.48 0.48 402 ✓ ★ AL14021A 192.15 192.66 0.51 401 ✓ ★	
AL14021A 192.15 192.06 0.31 401	
AL14021A 208.48 208.72 0.24 34 **	
AL14021A 209.11 209.28 0.17 33 ✓ *	
AL14021A 210.87 211.11 0.24 22 *	
AL14021A 217.97 218.19 0.22 1 ✓ *	
AL14022 11.32 11.9 0.58 402 ✓	✓
AL14022 11.9 12.9 1 35 ✓	✓
AL14022 13.5 13.9 0.4 34 ✓ ✓	*
AL14022 13.9 14.9 1 33 ✓	√
AL14022 14.9 15.76 0.86 31	√
AL14022 16.01 17.13 1.12 22 AL14022 17.13 17.65 0.52 21 AL14022 1.713 17.65 0.52 21 AL14022 1.713 1.765 0.52 21 AL14022 1.713 1.713 1.715 0.52 21 AL14022 1.715 0.71	√
ALI4022 17.15 17.05 0.52 21	<u> </u>
AL14022 17.75 10.75 1 12	<u> </u>
AL14022 18.73 19.72 0.99 11 ✓ AL14023A 156.19 156.58 0.39 41 ✓	<u> </u>
AL14023A 158.98 159.29 0.31 40 *	
AL14023A 156.58 155.25 0.31 40 ** AL14023A 164.64 165.81 1.17 35 **	
AL14026 124.09 125.42 1.33 42 ✓	✓
AL14026 125.97 129.12 3.15 41 ✓	✓
AL14026 139.25 140.01 0.76 35 ✓	✓
AL14026 140.01 142.15 2.14 34 ✓	×
AL14026 142.15 144.2 2.05 31 🗸	×
AL14026 144.2 145.35 1.15 21 🗸	*
AL14026 145.35 146.71 1.36 12 🗸	✓
AL14026 146.71 147.94 1.23 11 ✓	*
AL14028 49.44 51.36 1.92 42 ✓ ×	
AL14028 51.77 54.23 2.46 41 ✓ ★ AL14028 56.22 57.29 1.07 35 ✓ ★	
761-1020 30:22 37:23 1:07 33	
AL14028 57.76 59.01 1.25 32 ✓ ★ AL14028 59.08 59.9 0.82 31 ✓ ★	
AL14028 59.08 59.9 0.82 31	
AL14028 60.62 60.47 0.39 22	
AL14028 62.71 63.24 0.53 12 *	
AL14028 63.24 63.99 0.75 11 *	
AL14030 94.42 94.98 0.56 5 *	
AL14030 97.19 97.96 0.77 422 ✓ ×	
AL14030 98.19 98.45 0.26 421 ✓	17 of 20

Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
AL14030	98.45	101.34	2.89	41	✓	×	
AL14030	101.94	102.94	1	35	✓	*	
AL14030	102.94	103.06	0.12	34	✓	*	
AL14030	103.43	104.44	1.01	32	✓	*	
AL14030	104.44	105.16	0.72	31	✓	*	
AL14030	105.49	106.95	1.46	2	✓	*	
AL14031	5.27	6.77	1.5	42	✓	*	
AL14031	7.07	20.57	13.5	41	√	√	✓
AL14031	20.57	20.95	0.38	402	∀	se se	
AL14031	20.95	21.11	0.16	401	▼	*	
AL14031 AL14031	21.11 21.83	21.83 22.48	0.72 0.65	35 34	→	<u>~</u> ✓	*
AL14031 AL14031	23.22	23.6	0.88	33	→	<u> </u>	*
AL14031	24.74	25.42	0.68	32	· ✓	<u> </u>	√
AL14031	25.61	26.37	0.76	31	✓	√	✓
AL14031	26.96	28.27	1.31	2	✓	✓	✓
AL14031	28.94	29.67	0.73	1	✓	✓	✓
AL14031A	0.86	2.16	1.3	5	✓	*	
AL14031A	23.16	25.15	1.99	41	✓	×	
AL14031A	25.35	25.95	0.6	35	✓	*	
AL14031A	25.95	26.14	0.19	34	✓	*	
AL14031A	26.14	26.34	0.2	33	✓	x	
AL14031A	28.84	30.13	1.29	32	✓	*	
AL14031A	30.13	31.42	1.29	31	✓	*	
AL14031A	31.42	32.29	0.87	2	✓	*	
AL14031A	32.88	33.31	0.43	1	✓	*	
AL14032	13.92	14.14	0.22	74	√	<u> </u>	
AL14032	16.44	16.85	0.41	73	∀	*	
AL14032	18.74	19.39	0.65	72	▼	*	
AL14032 AL14032	23.3 42	25.6 42.22	2.3 0.22	71 67	→	*	
AL14032 AL14032	42.76	43.03	0.27	66	✓	*	
AL14032 AL14032	48.25	48.67	0.42	65	· · · · · · · · · · · · · · · · · · ·	*	
AL14032	50.92	51.84	0.92	64	· ✓	*	
AL14032	55.22	56.08	0.86	63	✓	*	
AL14032	60.14	60.59	0.45	62	✓	*	
AL14032	62.16	62.85	0.69	61	✓	*	
AL14032	96.41	96.69	0.28	5	✓	×	
AL14032	109.16	109.98	0.82	42	✓	×	
AL14032	113.86	119.19	5.33	41	✓	*	
AL14032	119.31	119.46	0.15	40	✓	*	
AL14032	119.46	120.31	0.85	35	✓	*	
AL14032	121.12	121.43	0.31	33	✓	*	
AL14032	121.63	122.89	1.26	32	✓	<u> </u>	
AL14032	123.42	124.12	0.7	31	✓	*	
AL14032	124.74	124.89	0.15	2	✓););	
AL14032	128.86	129.41	0.55	12	∀	*	
AL14032 AL14033	130.67 27.3	131.11	0.44 0.43	<u>11</u> 5	▼	*	
AL14033 AL14033	30.34	27.73 30.74	0.43	422	→	*	
AL14033 AL14033	31.08	35.53	4.45	422	✓	*	
AL14033	35.53	35.76	0.23	40	✓	*	
AL14033	35.9	36.67	0.77	35	✓	*	
AL14033	36.84	37.8	0.96	31	✓	*	
AL14033	38.46	38.59	0.13	22	✓	*	
AL14033	39.31	39.73	0.42	21	✓	3 0	
AL14034	198.16	198.4	0.24	5	✓	*	
AL14034	202.77	202.96	0.19	422	✓	×	
AL14034	203.81	204.01	0.2	421	✓	x	
AL14034	204.01	206.7946	2.7845838	41	✓	35	
AL14034	207.19	207.88	0.69	35	✓	*	
AL14034	208.11	208.58	0.47	31	✓	*	
AL14035	30.77	30.98	0.21	5	✓	✓	√ 19 of 20

Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
AL14035	33.58	34.34	0.76	42	✓	✓	✓
AL14035	34.41	36.8	2.39	41	✓	✓	✓
AL14035	37.43	38.45	1.02	3	✓	×	
AL14035	40.78	40.88	0.1	22	✓	*	
AL14035	41.04	41.75	0.71	21	✓	*	
AL14035A	32.4	32.54	0.14	5	√	.	
AL14035A	35.06	35.57	0.51	42	√	.	
AL14035A	35.72	38.12	2.4	41	√	<u> </u>	
AL14035A	42.59	42.91	0.32	2	∀	x x	
AL14035A	68.52	68.68	0.16	12	▼	*	
AL14035A AL14036	69.97 62.67	70.07 63.27	0.1 0.6	<u>11</u> 5	▼	<u> </u>	
AL14036	65.61	66.13	0.52	42	· · · · · · · · · · · · · · · · · · ·	*	
AL14036	66.37	68.87	2.5	41	· ✓	3 6	
AL14036	74.34	74.48	0.14	22	✓	x	
AL14036	74.85	75.25	0.4	21	✓	x	
AL14036	98.63	99.62	0.99	12	✓	*	
AL14036	99.93	100.24	0.31	11	✓	×	
AL14037	9.86	10.57	0.71	5	✓	se	
AL14037	13.69	14.42	0.73	42	✓	✓	✓
AL14037	14.42	16.68	2.26	41	✓	✓	✓
AL14052	30.8	31.61	0.81	422	✓	✓	✓
AL14052	33.42	33.71	0.29	4212	✓	✓	✓
AL14052	38.53	38.81	0.28	4211	✓	<u>√</u>	✓
AL14052	41.4	42.21	0.81	41	✓	✓	✓
AL14052	42.21	42.5	0.29	402	√		
AL14052	42.81	43.05	0.24	401	√	<u> </u>	
AL14052A	30.74	31.4	0.66	422	∀	×	
AL14052A	33.92	34.17	0.25	4212	▼	*	
AL14052A AL14052A	38.87 41.81	39.14 42.86	0.27 1.05	4211 41	▼	*	
AL14052A AL14053	87.44	87.68	0.24	422	→	<u> </u>	
AL14053	92.5	92.73	0.24	422	→	<u> </u>	
AL14053	97.94	98.17	0.23	412	✓	3 2	
AL14053	101.86	101.99	0.13	411	✓	,x	
AL14054	53.72	54.19	0.47	4222	✓	3¢	
AL14054	54.61	55.09	0.48	4221	✓	×	
AL14054	58.01	58.43	0.42	421	✓	×	
AL14054	81.27	81.71	0.44	412	✓	3 ¢	
AL14056	23.21	24.07	0.86	422	✓	×	
AL14056	27.07	27.46	0.39	421	✓	3¢	
AL14056	28.9	31.04	2.14	41	✓	3C	
AL14057	57.32	57.94	0.62	422	✓	*	
AL14057	60.95	61.48	0.53	421	√	*	
AL14057	62.61	64.72	2.11	41	✓	*	
AL14057	65.95	66.33	0.38	402	∀	×	
AL14057	66.64	66.81 60.68	0.17	401	∀	*	
AL14058 AL14058	60.47 63.54	65.28	0.21 1.74	421 41	▼	*	
AL14058 AL14058	65.28	65.57	0.29	41	✓	<u> </u>	
AL14066	10.15	11.05	0.29	422	<i>→</i>	<u>√</u>	✓
AL14066	11.05	11.96	0.91	421	✓	✓	✓
AL14066	11.96	14.92	2.96	41	✓	✓	✓
AL14066	15.82	16.01	0.19	35	✓	✓	✓
AL14066	16.01	16.13	0.12	34	✓	✓	✓
AL14066	16.13	16.76	0.63	33	✓	✓	✓
AL14066	16.76	17.75	0.99	32	✓	✓	✓
AL14066	18.48	18.9	0.42	31	✓	✓	✓
AL14066	19.34	19.51	0.17	22	✓	<u>√</u>	✓
AL14066	19.57	19.71	0.14	21	✓	<u>√</u>	√
AL14066	19.84	21.66	1.82	12	✓	<u> </u>	√
AL14066	21.66	23.49	1.83	11	√	<u> </u>	√
AL14076	35.61	37.4	1.79	42	✓	▼	2.10 of 20

Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
AL14076	37.4	40.03	2.63	41	✓	✓	✓
AL14076	40.03	40.48	0.45	402	✓	3c	
AL14076	40.91	41.85	0.94	35	✓	✓	*
AL14076	41.85	42.39	0.54	34	✓	√	*
AL14076	46.46	46.98	0.52	22	✓	<u>√</u>	*
AL14076	48.43	49.16	0.73	21	✓	<u>√</u>	*
AL14076	49.23	50.47	1.24	12	✓	<u>√</u>	✓
AL14076	50.47	50.67	0.2	11	√		
ALBS004	18.95	20.06	1.11	422	√	<u> </u>	
ALBS004	20.06	21.44	1.38	421	∀	x x	
ALBS004	21.54	23.9	2.36	41	∀	*	
ALBS004 ALBS004	25.06 28.97	26.93 29.98	1.87 1.01	35 22	,	*	
ALBS004 ALBS004	30.07	30.66	0.59	21	√	*	
ALBS004 ALBS005	20.23	21.01	0.78	422	· ✓	<u></u>	
ALBS005	21.01	21.59	0.78	421	· ✓	3c	
ALBS005	21.59	24.11	2.52	41	· ✓	JC .	
ALBS005	24.63	25.54	0.91	35	✓	*	
ALBS005	25.7	26.34	0.64	34	✓	×	
ALBS005	26.79	27.02	0.23	33	✓	*	
ALBS005	29.58	30.11	0.53	22	✓	Jc .	
ALBS005	30.21	31.36	1.15	21	✓	x	
ALBS005	31.41	31.64	0.23	12	✓	x	
ALBS005	32.15	33.11	0.96	11	✓	x.	
ALBS006	12.91	13.1	0.19	5	✓	3c	
ALBS006	19.26	21.1	1.84	42	✓	3c	
ALBS006	21.1	23.84	2.74	41	✓	*	
ALBS006	24.15	25.23	1.08	35	✓	*	
ALBS006	25.31	26.27	0.96	34	✓	sc	
ALBS006	26.77	27.06	0.29	33	✓	.	
ALBS006	27.44	27.83	0.39	31	✓	\$c	
ALBS006	28.68	29.6	0.92	22	✓	3 0	
ALBS006	29.6	30.26	0.66	21	√	*	
ALBS006	30.64	32.07	1.43	12	√	* *	
ALBS006	32.07	32.71	0.64	11	∀	<u>*</u> ✓	✓
ALCORE2	0.72 2.58	2.58 3.72	1.86	41 40	→	<u> </u>	▼
ALCORE2	3.72	4.72	1.14	35	→	<u> </u>	· ·
ALCORE2	4.95	5.52	0.57	34	· ✓	<u> </u>	→
ALCORE2	6.29	7.02	0.73	31	· ✓	<u> </u>	✓
ALCORE2	7.02	7.79	0.77	12	✓	<u> </u>	✓
ALCORE2	7.79	8.66	0.87	11	✓	✓	✓
ALCORE3	0.59	3.71	3.12	41	✓	✓	✓
ALCORE3	3.71	4.06	0.35	40	✓	✓	✓
ALCORE3	4.87	5.87	1	35	✓	✓	✓
ALCORE3	6.37	7.69	1.32	22	✓	✓	✓
ALCORE3	7.69	8.69	1	21	✓	✓	✓
ALCORE3	8.69	9.69	1	12	✓	✓	✓
ALCORE3	9.69	10.53	0.84	11	✓	<u>√</u>	✓
ALCORE6	6.94	7.77	0.83	42	✓	<u> </u>	√
ALCORE6	10.34	10.93	0.59	35	√	<u>√</u>	√
ALCORE7	11.62	12.59	0.97	42	√	<u> </u>	√
ALCORE7	15.78	17.96	2.18	41	√	<u>√</u>	√
ALCORE7	17.96	18.61	0.65	40	√	<u>√</u>	Y
ALCORE7	19.13	19.55	0.42	35	√	<u>√</u>	V
ALCORES	3.2	4.91	1.71	41	∀	<u> </u>	*
ALCORES	4.91	5.61	0.7	40 35	∀	*	^
ALCORE8 ALCORE9	5.81 2.432	7.4 3.432	1.59 1	42	→	<u> </u>	✓
ALCORE9	3.432	7.502	4.07	42	→	<u> </u>	· ·
ALCORE9	7.592	7.502	0.4	402	√	<u> </u>	→
ALCORE9	8.092	8.482	0.39	402	√		√
ALCORE9	8.542	10.102	1.56	35	· ✓	✓	✓
	0.072	_002	1.50	33	ı.		20 of 20

Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
ALCORE9	12.85	13.41	0.56	22	✓	✓	✓
ALCORE9	13.41	14.41	1	21	✓	✓	✓
ALCORE9	14.91	15.91	1	12	✓	✓	✓
ALCORE9	15.91	16.71	0.8	11	✓	✓	✓
ALLOX01	2.9	3.48	0.58	421	✓	✓	×
ALLOX01	3.96	6.22	2.26	41	✓	✓	✓
ALLOX01	7.21	7.68	0.47	35	✓	<u> </u>	✓
ALLOX02	6.25	6.9	0.65	421	✓	<u>√</u>	*
ALLOX02	6.9	9.94	3.04	41	✓	<u> </u>	✓
ALLOX02	10.34	10.79	0.45	35	✓	✓	✓
ALLOX04	10.84	11	0.16	12	✓	*	
ALLOX05	37.55	37.75	0.2	42	✓	<u>√</u>	√
ALLOX05	42.3	43.57	1.27	41	✓	<u> </u>	√
ALLOX05	43.88	44.07	0.19	402	✓	<u> </u>	√
ALLOX06	5.1	6.24	1.14	12	√	√	✓
ALLOX06	6.44	6.75	0.31	11	✓	<u>*</u>	
ALLOX07	0.7	3.2	2.5	41	√	<u> </u>	✓
ALLOX07	3.2	4.2	1	35	∀	<u> </u>	V
ALLOX07	4.2	5.12	0.92	34	∀	<u> </u>	•
ALLOX07	5.32	6.21	0.89	31	∀	<u> </u>	x
ALLOX07	25.23	26.16	0.93	12	∀	·	V
ALLOX07	26.53	26.94 8.69	0.41 0.5	11 422	∀	<u>*</u>	✓
ALLOX09	8.19		0.5		→	<u> </u>	▼
ALLOX09 ALLOX09	8.69 9.19	9.19 13.19	0.5 4	421 41	∀	<u> </u>	V ✓
ALLOX09	13.19	14.19	1	35	√	<u> </u>	→
ALLOX09	14.19	15.18	0.99	34	· · · · · · · · · · · · · · · · · · ·	<u> </u>	
ALLOX09	15.85	15.16	0.15	32	→	*	•
ALLOX09	17.13	17.37	0.13	22	· ·	*	
ALLOX09	18.51	19.01	0.24	21	· ✓	<u>√</u>	✓
ALLOX09	19.01	20.08	1.07	12	✓		✓
ALLOX09	20.08	20.68	0.6	11	✓	✓	✓
ALLOX10	0.09	0.69	0.6	42	✓	✓	✓
ALLOX10	0.77	5.77	5	41	✓	✓	✓
ALLOX10	5.77	6.77	1	402	✓	✓	✓
ALLOX10	6.77	7.27	0.5	401	✓	✓	✓
ALLOX10	7.27	8.27	1	35	✓	✓	✓
ALLOX10	8.27	9.55	1.28	34	✓	✓	✓
ALLOX10	9.55	10.12	0.57	33	✓	✓	✓
ALLOX10	10.12	10.56	0.44	32	✓	✓	✓
ALLOX10	11.22	11.5	0.28	31	✓	✓	✓
ALLOX10	11.97	13.28	1.31	22	✓	✓	✓
ALLOX10	13.28	14.28	1	21	✓	✓	✓
ALLOX10	14.28	15.28	1	12	✓	✓	✓
ALLOX10	15.28	16.4	1.12	11	✓	✓	✓
ALLOX11	3.99	5.13	1.14	35	√	<u> </u>	✓
ALLOX11	5.13	5.63	0.5	34	√	√	√
ALLOX11	5.63	6.26	0.63	33	✓	<u>√</u>	√
ALLOX11	6.26	6.58	0.32	32	✓	<u>√</u>	✓
ALLOX11	6.88	7.2	0.32	31	✓	<u>√</u>	*
ALLOX11	7.27	7.77	0.5	22	✓	<u>√</u>	√
ALLOX11	7.77	8.77	1	21	✓	<u>√</u>	√
ALLOX11	9.27	10.27	1	12	✓	<u>√</u>	√
ALLOX11	10.27	11.02	0.75	11	✓	<u> </u>	√
ALLOX13	5.88	6	0.12	42	√	<u> </u>	√
ALLOX13	6.48	7.14	0.66	41	√	<u> </u>	∀
ALLOX13	7.43	7.61	0.18	40	√	<u>√</u>	√
ALLOX13	8	9	1	35	✓	<u>√</u>	✓
ALLOX13	9	9.5	0.5	34	∀	<u> </u>	✓
ALLOX13	9.5	10.38	0.88	33	∀	· · · · · · · · · · · · · · · · · · ·	Y
ALLOX13	10.38	10.63	0.25	32	✓	<u>*</u>	✓
ALLOX13	10.63	11.63	1	31	∀	<u> </u>	▼
ALLOX13	11.63	12.13	0.5	22	Y	<u> </u>	21 of 20

Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
ALLOX13	12.13	13.26	1.13	21	✓	✓	✓
ALLOX13	13.76	14.76	1	12	✓	✓	✓
ALLOX13	14.76	16.11	1.35	11	✓	✓	✓
ALLOX14	8.62	9.35	0.73	35	✓	<u> </u>	✓
ALLOX14	10.36	11.1	0.74	34	✓	<u> </u>	✓
ALLOX14	11.49	12.07	0.58	32	✓	<u>√</u>	✓
ALLOX14	12.07	12.81	0.74	31	✓	<u>√</u>	√
ALLOX14	12.85	13.61	0.76	22	√	<u>√</u>	√
ALLOX14	13.71	14.3	0.59	21	✓	<u>√</u>	✓
ALLOX14	14.42	15.08	0.66	12	√	<u>√</u>	∀
ALLOX14	15.08	16.12	1.04	11	✓	<u>√</u>	*
ALCORE3	0.59	3.71	3.12	41	∀	<u> </u>	*
ALCORE3	3.71	4.06	0.35	40	▼	<u> </u>	•
ALCORE3	4.87	5.87	1 22	35	→	<u> </u>	▼
ALCORE3	6.37	7.69	1.32	22	▼	<u> </u>	▼
ALCORE3	7.69 8.69	8.69 9.69	1	21 12	→	<u> </u>	· ·
ALCORE3 ALCORE3	9.69	10.53	0.84	11	→	<u> </u>	√
ALCORES ALCORES	6.94	7.77	0.83	42	→	<u> </u>	
ALCORE6	10.34	10.93	0.83	35	→	<u>·</u>	· ·
ALCORE7	11.62	12.59	0.39	42	→	<u> </u>	· ·
ALCORE7	15.78	17.96	2.18	42	√	<u> </u>	·
ALCORE7	17.96	18.61	0.65	40	√	<u> </u>	→
ALCORE7	19.13	19.55	0.42	35	✓		✓
ALCORE8	3.2	4.91	1.71	41	✓	√	✓
ALCORE8	4.91	5.61	0.7	40	✓	✓	×
ALCORE8	5.81	7.4	1.59	35	✓	*	
ALCORE9	2.432	3.432	1	42	✓	✓	✓
ALCORE9	3.432	7.502	4.07	41	✓	✓	✓
ALCORE9	7.592	7.992	0.4	402	✓	✓	✓
ALCORE9	8.092	8.482	0.39	401	✓	✓	✓
ALCORE9	8.542	10.102	1.56	35	✓	✓	✓
ALCORE9	12.85	13.41	0.56	22	✓	✓	✓
ALCORE9	13.41	14.41	1	21	✓	✓	✓
ALCORE9	14.91	15.91	1	12	✓	✓	✓
ALCORE9	15.91	16.71	0.8	11	✓	✓	✓
ALLOX01	2.9	3.48	0.58	421	✓	✓	×
ALLOX01	3.96	6.22	2.26	41	✓	✓	✓
ALLOX01	7.21	7.68	0.47	35	✓	<u> </u>	✓
ALLOX02	6.25	6.9	0.65	421	✓	<u> </u>	*
ALLOX02	6.9	9.94	3.04	41	✓	<u>√</u>	√
ALLOX02	10.34	10.79	0.45	35	✓	√	✓
ALLOX04	10.84	11	0.16	12	✓	*	
ALLOX05	37.55	37.75	0.2	42	✓	<u>√</u>	√
ALLOX05	42.3	43.57	1.27	41	✓	<u>√</u>	√
ALLOX05	43.88	44.07	0.19	402	∀	<u> </u>	✓
ALLOX06	5.1	6.24	1.14	12	∀	<u>*</u>	*
ALLOX06	6.44	6.75	0.31	11	∀	<u>*</u>	✓
ALLOX07	0.7	3.2	2.5	41	∀	<u> </u>	∀
ALLOX07	3.2	4.2	1	35	▼	<u> </u>	∀
ALLOX07	4.2 5.32	5.12	0.92 0.89	34 31	✓	<u> </u>	*
ALLOX07 ALLOX07	25.23	6.21 26.16	0.89	12	✓	<u> </u>	× /
ALLOX07 ALLOX07	26.53	26.16	0.93	11	→	<u>, , , , , , , , , , , , , , , , , , , </u>	*
ALLOX07	8.19	8.69	0.41	422	V	<u>~</u> ✓	✓
ALLOX09	8.69	9.19	0.5	422	→	<u> </u>	· ·
ALLOX09	9.19	13.19	4	421	√	<u> </u>	√
ALLOX09	13.19	14.19	1	35	· ✓	<u> </u>	· ✓
ALLOX09	14.19	15.18	0.99	34	✓	<u>·</u>	✓
ALLOX09	15.85	16	0.15	32	✓	3 C	
ALLOX09	17.13	17.37	0.24	22	✓	sc	
ALLOX09	18.51	19.01	0.5	21	✓	✓	✓
ALLOX09	19.01	20.08	1.07	12	✓	✓	✓
					L		o 22 of 20

Hole	From	То	Thickness	Seam	Geophysically logged	Sampled	JORC POB
ALLOX09	20.08	20.68	0.6	11	✓	✓	✓
ALLOX10	0.09	0.69	0.6	42	✓	✓	✓
ALLOX10	0.77	5.77	5	41	✓	✓	✓
ALLOX10	5.77	6.77	1	402	✓	✓	✓
ALLOX10	6.77	7.27	0.5	401	✓	✓	✓
ALLOX10	7.27	8.27	1	35	✓	✓	✓
ALLOX10	8.27	9.55	1.28	34	✓	✓	✓
ALLOX10	9.55	10.12	0.57	33	✓	✓	✓
ALLOX10	10.12	10.56	0.44	32	✓	✓	✓
ALLOX10	11.22	11.5	0.28	31	✓	✓	✓
ALLOX10	11.97	13.28	1.31	22	✓	✓	✓
ALLOX10	13.28	14.28	1	21	✓	✓	✓
ALLOX10	14.28	15.28	1	12	✓	✓	✓
ALLOX10	15.28	16.4	1.12	11	✓	✓	✓
ALLOX11	3.99	5.13	1.14	35	✓	✓	✓
ALLOX11	5.13	5.63	0.5	34	✓	✓	✓
ALLOX11	5.63	6.26	0.63	33	✓	✓	✓
ALLOX11	6.26	6.58	0.32	32	✓	✓	✓
ALLOX11	6.88	7.2	0.32	31	✓	✓	*
ALLOX11	7.27	7.77	0.5	22	✓	✓	✓
ALLOX11	7.77	8.77	1	21	✓	✓	✓
ALLOX11	9.27	10.27	1	12	✓	✓	✓
ALLOX11	10.27	11.02	0.75	11	✓	✓	✓
ALLOX13	5.88	6	0.12	42	✓	✓	✓
ALLOX13	6.48	7.14	0.66	41	✓	✓	✓
ALLOX13	7.43	7.61	0.18	40	✓	✓	✓
ALLOX13	8	9	1	35	✓	✓	✓
ALLOX13	9	9.5	0.5	34	✓	✓	✓
ALLOX13	9.5	10.38	0.88	33	✓	✓	✓
ALLOX13	10.38	10.63	0.25	32	✓	3€	
ALLOX13	10.63	11.63	1	31	✓	✓	✓
ALLOX13	11.63	12.13	0.5	22	✓	✓	✓
ALLOX13	12.13	13.26	1.13	21	✓	✓	✓
ALLOX13	13.76	14.76	1	12	✓	✓	✓
ALLOX13	14.76	16.11	1.35	11	✓	✓	✓
ALLOX14	8.62	9.35	0.73	35	✓	✓	✓
ALLOX14	10.36	11.1	0.74	34	✓	✓	✓
ALLOX14	11.49	12.07	0.58	32	✓	✓	✓
ALLOX14	12.07	12.81	0.74	31	✓	✓	✓
ALLOX14	12.85	13.61	0.76	22	✓	✓	✓
ALLOX14	13.71	14.3	0.59	21	✓	✓	✓
ALLOX14	14.42	15.08	0.66	12	✓	✓	✓
ALLOX14	15.08	16.12	1.04	11	✓	✓	*

APPENDIX B – JORC Table 1

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	 Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information. 	 HQ core was used to obtain coal samples of seams and plies for raw and proximate analysis. All holes were geophysically logged using down-hole wireline tools. Calibration and quality appear to be in line with industry standards and seam correlation and characteristics are readily discernible. Sampling and sub-sampling of core for analysis provides accurate and reliable adherence to lithological boundaries and provides sufficient information to determine seam and ply quality.
Drilling techniques	 Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.). 	 All coal quality holes were cored (partially or fully) using a HQ3 size barrel, 61.1 millimetres core diameter
Drill sample recovery	 Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material. 	 Drill sample recoveries are assessed both on a linear core measurement and a mass recovery basis (dispatch mass/lab mass/calculated expected mass) A linear/mass recovery cut-off of 95% generally applies to points of observation, although samples of <95% have been assessed individually and a determination has been made regarding the samples representivity of the seam from which it is taken. Loss intervals were determined after reconciliation to geophysical logs and lab determined mass recovery.

Criteria	JORC Code explanation	Commentary
Sub- sampling techniques and sample preparation	 Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography. The total length and percentage of the relevant intersections logged. If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry. For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. Whether sample sizes are appropriate to the grain size of the material being sampled. 	 Geological logging is available for all drill holes used within the model build and resource estimate. Quality is of a good standard and depths have been reconciled to geophysics. Only fully cored holes have been drilled – no open holes have been drilled at Amaam North, however not all core is stored and maintained The total length of logged drill core is 9698m (114 drill holes) Core is split into lithological boundaries as per an accepted generic sampling protocol. Coal seams are not sampled in increments thicker than 1m, and seams are also sampled at any lithological changes or notable differences in coal brightness. Any stone partings in the seam in excess of 5cm are typically sampled separately. Roof, Floor and thicker partings are sampled (typically 20cm) for dilution.
Quality of assay data and laboratory tests	 The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established. 	 Coal quality testing is carried out within the SGS laboratories in Moscow under the direct supervision of A & B Mylec. The laboratory has been subjected to independent audit prior to the commencement of work for TIG. Coal quality is checked and collated by A & B Mylec before inclusion in the geological/coal quality models. A total of 68 holes within Project F have been assessed for coal quality
Verification of sampling and assaying	 The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes. Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. Discuss any adjustment to assay data. 	 The primary method for verification of the sampling intervals is through wireline geophysical logs. Corrected depths and seam nomenclature are supplied to the laboratories.

Criteria	JORC Code explanation	Commentary
Location of data points	 Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. Specification of the grid system used. Quality and adequacy of topographic control. 	 The survey equipment used was a GNSSJAVAD Triumph-1. Survey included removal of snow to ground surface, and location of the collar. (UTM60 north – WGS84) Four pairs of 80cm IKONOS stereo imagery were used to create the 2m DTM and 5m contours covering 437 km2 over Amaam North. This is considered adequate for the purposes of reporting resources. Reconciliation of topographic height to surveyed collar height was completed and showed acceptably small offset. An updated suite of topographic data has been collected during the 2014 summer period, however the processing of this data is as yet incomplete.
Data spacing and distribution	 Data spacing for reporting of Exploration Results. Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. Whether sample compositing has been applied. 	 Drill holes within Project F central area have been drilled at approximately 250m apart along strike and down dip. Given the strong degree of correlation within the drill holes (in the majority of seams and all key economic seams), Resolve are satisfied that the continuity of structure and grade is strongly supported within the Indicated and Measured classification Areas. The Eastern extension of Project F has drill spacing of 800-1500m. Additional observed structure in these drill holes resulted in only Inferred Resources being considered.
Orientation of data in relation to geological structure	 Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material. 	 All drill holes are vertically drilled. Dip is estimated to be approximately 8-10 degrees and coal is modelled using these apparent dips. Regional structure is determined through cross sectional analysis and appropriate buffers around known faults apply, within which resources are reported within the inferred category. All seam and parting thicknesses referred to are apparent thicknesses.
Sample security	The measures taken to ensure sample security.	 Resolve has observed the collection of samples, and the transfer procedure into Anadyr from Beringovsky. Resolve is satisfied that the security of sampling is as good as is readily achievable within the operating environment.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	 Resolve completed an audit of the full process of drilling, data collection, interpretation and storage during a field visit in February 2014. No significant issues were found and all processes, geologists and software were fit for task.

Section 3 Estimation and Reporting of Mineral Resources

Criteria	JORC Code explanation	Commentary
Database integrity	 Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. Data validation procedures used. 	 All coal seam depths and sample numbers have been independently verified and corrected. Any remaining transcription errors may have no bearing on the process of resource estimation.
Site visits	 Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is the case. 	 The competent person undertook a field visit to Amaam North in 2010. Time was spent verifying the location and quality of outcrop and reviewing nearby historical Drill hole data. The competent person conducted a further 3 week field visit in February 2014, where a comprehensive validation and audit of data collection and post processing was undertaken.
Geological interpretatio n	 Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. Nature of the data used and of any assumptions made. The effect, if any, of alternative interpretations on Mineral Resource estimation. The use of geology in guiding and controlling Mineral Resource estimation. The factors affecting continuity both of grade and geology. 	 Resolve consider the interpretation of the geology to be highly accurate. Precise location, orientation and density of modelled faults requires additional infill drilling to determine, however the geology is tightly controlled in the context of the JORC classification in which it is estimated. Deterioration of the lower (3/2/1) coal seams is well documented within the drill holes. Modelled quality within these seams reflects the deteriorating quality from east to west and appropriate thickness and ash (%) cut-off has been applied.
Dimensions	The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.	The coal resources reported extend along strike approximately 11km. (indicated/measured Resources extend approximately 4.5km) Inferred resources are extrapolated to a maximum of approximately 1.2km from the coal sub crop. The coal seams appear to steepen in dip on the north eastern region of the reported resource.
Estimation and modelling techniques	 The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used. The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data. The assumptions made regarding recovery of by-products. 	• The estimation was undertaken using the computer model generated in Vulcan and Micromine Modelling software. Seam thickness grids and in situ density grids were limited by resource polygon areas by the software. Resources were limited below the gridded base of weathering surface. 'Thermal' coal was also estimated in the zone below the estimated base of quaternary (1m below topography) and the base of weathering. A minimum seam thickness of 0.3m was applied to the 'open cut' resources and 1.2m to potential 'underground' resources. Underground resources were estimated for a working section of Seam 41 and 42 (or composites thereof) only at depth greater than 150m.

Criteria	JORC Code explanation	Commentary
Moisture	 Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation). In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed. Any assumptions behind modelling of selective mining units. Any assumptions about correlation between variables. Description of how the geological interpretation was used to control the resource estimates. Discussion of basis for using or not using grade cutting or capping. The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available. Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content. 	 All coal plies were included in the resource estimate Block models were estimated at 50m x 50m spacing. Resolve consider this appropriate for the dimensions of the deposit and the typical drill hole spacing. This spacing is too large for LOX drilled areas, however the coverage of this LOX drilling is not considered wide enough at this stage to warrant the generation of a smaller subset model, however this will be required upon completion of more widespread LOX coverage. Previous Resource estimates were completed in 2013. Reconciliation to these estimates was undertaken in areas where no further drilling has occurred 50% raw ash cut-off has been utilised for coal plies, this serves to reflect within the resource numbers the total likely reservable tonnes which have economic potential, and the representative coal quality. Coal tonnages are estimated using an in situ density, calculated using the Preston-Sanders formula for In-situ RD. The in situ moisture calculations required to provide this figure were performed by A & B
Cut-off parameters	The basis of the adopted cut-off grade(s) or quality parameters applied.	 Mylec on a sample basis. A 50% ash cut-off applies on a seam/ply composite basis. The impact on resources by this cut-off is negligible. 30cm minimum seam thickness for cut-off (plies have been assessed for thickness as a composite when they are not separated by a stone parting) 120cm minimum thickness for underground seams, based on a parent composite of the 41/42 seams (with their associated splits and stone partings as appropriate (no partings >30cm or greater than the adjacent coal seam). No other plies have been considered for underground extraction at this stage.
Mining factors or assumptions	 Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions 	A 30cm seam cut off was used, assuming an in-pit truck shovel operation. Seams below 30cm thickness are not considered practical to mine by this method. Operation is an arctic climate may influence this further in the practical application of mining techniques, however Resolve have not adjusted the thickness cut-off on this basis. Coal quality includes thin coal seam partings and is therefore not indicative of a final product density/tonnage in some cases (individual seams are likely to require no washing)

Criteria	JORC Code explanation	Commentary
	made.	 A 1.2m cut-off has been applied to underground resources. This required the modelling of an underground working section (seam 4). 1.2m is the minimum working height within neighbouring mines and has been implemented in this case. The actual optimal working height of an underground mine within project F may vary from this.
Metallurgical factors or assumptions	The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	• N/A
Environmen- tal factors or assumptions	• Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfield project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	economic extraction within Project F.
Bulk density	 Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples. The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit. Discuss assumptions for bulk density estimates used in the evaluation process of the different materials. 	 Both laboratory RD, and Apparent RD (ARD) were determined by SGS. A Preston Sanders equation was then applied using in-situ moisture (calculations provided on a sample basis by AB Mylec). This provides an industry accepted In situ density for reporting of tonnages. In situ RD should reconcile well with ARD, This is the case with these samples.
Classificatio n	 The basis for the classification of the Mineral Resources into varying confidence categories. Whether appropriate account has been taken of all relevant factors 	 Drill hole data spacing is adequate for measured resources to be reported across the reported area, in accordance with the current coal guideline (2004) spacing suggestions. Given the strong correlation

Criteria	JORC Code explanation	Commentary
	 (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data). Whether the result appropriately reflects the Competent Person's view of the deposit. 	 within the densely drilled areas of Project F, a geostatistical study has not been deemed necessary for this area. Indicated and inferred areas are well supported by drilling and the geology is not complex. Inferred areas do show the potential for structural complexity and although drill spacing is generally <1000m in the east, the Inferred classification here is a justifiable one.
Audits or reviews	The results of any audits or reviews of Mineral Resource estimates.	No external reviews or audits have been carried out on this resource model. Internal reviews to test the robustness of the model have been carried out, including reconciliation to drill hole data.
Discussion of relative accuracy/ confidence	 Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate. The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available. 	 No production data is available to provide reconciliation with tonnes and grade to coal quality reported within individual JORC classifications. The estimates are considered to be accurate to within their respective confidence classification. Reconciliation within the central Area of Project F to the models produced in 2013 (models produced in different modelling software by a different consultancy), is very strong and confirms the robustness of the model and the input data.